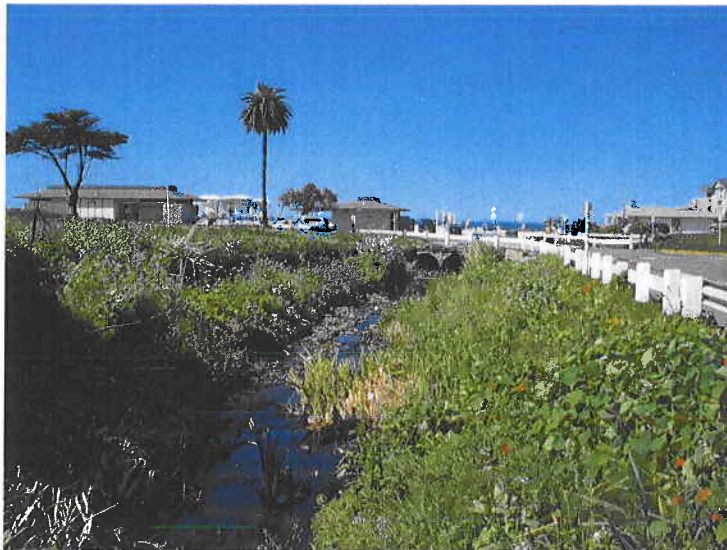


COTTONWOOD CREEK/MOONLIGHT BEACH



Hydrology and Facilities Analysis Summary

Prepared for:

CITY OF ENCINITAS

Prepared By:

NOLTE ASSOCIATES, INC.

April 9, 2003

TABLE OF CONTENTS

<u>Section</u>	<u>Page</u>
1.0 Introduction.....	1
2.0 Hydrologic Analysis.....	1
3.0 Storm Drain Facilities Analysis	2
3.1 Existing conditions	2
3.2 Proposed alternatives	3
3.3 Proposed Fourth Street Storm Drain System	4

TABLES

TABLE 1	Hydrologic Summary
TABLE 2	Existing Conditions: Storm Drain Facilities Summary
TABLE 3	Proposed Alternatives: Storm Drain Facilities Summary

FIGURES

FIGURE 1	Storm Drain Facilities
----------	------------------------

APPENDICES

APPENDIX A	Existing Conditions: Natural Channel Hydraulic Calculations
APPENDIX B	Existing Conditions: Storm Drain Facilities Calculations
APPENDIX C	Proposed Alternatives: Storm Drain Facilities Calculations
APPENDIX D	Proposed Fourth Street Storm Drain System
APPENDIX E	Site Photographs

1.0 INTRODUCTION

The study area is in an urbanized location within the coastal plain of San Diego County in the City of Encinitas. The Cottonwood Creek watershed is bound by the Pacific Ocean to the west, Leucadia on the north, Cardiff on the south, and La Costa South on the east. The watershed drains westerly along Encinitas Boulevard through a series of storm drain pipes, natural channels, and streets until reaching Moonlight Beach.

This Hydrology and Facilities Analysis report for the Cottonwood Creek/Moonlight Beach area will briefly summarize our results up to this point.

2.0 HYDROLOGIC ANALYSIS

We have performed 3 separate analyses to help us determine what methodology fits best for the Cottonwood Creek watershed. Methodologies we used include the Modified Rational Method, the SCS Unit Hydrograph Method, and a combination to these two methods (Rational Method up to 640 acres then switch over to Unit Hydrograph Method). The results of these analyses allow us to bracket the upper and lower limits of peak flow rates.

We performed field reconnaissance on September 24 and 25, 2002. Watershed boundaries specified in the City of Encinitas' Master Drainage Plan were verified and revised accordingly. A 1"=800' scale street flow map provided by the City of Encinitas was also used in the determination and verification of the watershed boundaries. Existing land uses were also confirmed during these site visits.

We divided the watershed into subareas based on land use, soil type, topography, and critical flow locations. These critical flow locations include the large detention basin located near Quail Gardens Drive in the northeast corner of the watershed and the area from Highway 101 to the ocean outfall at Moonlight Beach. Our analysis includes the outflow of approximately 500 cubic feet per second (cfs) (SB&O Detention and Water Quality Basin Report dated February 16, 2001) from the detention basin that captures storm runoff from the 316-acre development. However, to generate 500 cfs while keeping the time of concentration at the approximate value listed in the SB&O report, land use and soil classification values may not be indicative of the actual site conditions in this area.

Table 1 summarizes the results from the three methods described above in addition to the results presented in the City of Encinitas Master Plan of Drainage (1992).

Table 1: Summary of Hydrologic R

Master Plan of Drainage (1992) ^{ated Method}				Location
Node #	Q ₁₀₀ (cfs)	Area	Area (AC)	
2006	380	1	172.4	Encinitas Blvd @ Princehouse Lane
2009	790	3	287.5	Encinitas Blvd @ Delphinium St.
2015	1500	7	804.5	Encinitas Blvd @ Quail Rd
2018	2200	1	1318.2	Encinitas Blvd @ West side I-5 ramps
2607	3250	1	2091.9	B St. @ 4 th St.

¹ Discrepancy in areas due to rounding

3.0 STORM DRAIN FACILITIES ANALYSIS

3.1 Existing Conditions

Using the results from the Unit Hydrograph analysis, the ocean outfall pipes, culverts, and natural channels within the Moonlight Beach/Cottonwood Creek area were evaluated for their hydraulic capacity. Based on the Hydrology and Water Quality Report for Cottonwood Creek (prepared by Nolte Associates, Inc. dated January 2003), approximately 960 cfs from Cottonwood Creek is captured by the existing 96-inch culvert on the eastern side of Vulcan Avenue. This flow confluences with the 204 cfs inflow near Second Avenue. The combined flow of 1164 cfs was used as the design discharge to analyze the Third Street culvert crossing and the channel capacity upstream of Third Street. Near Fourth Street, an additional 90 cfs joins the creek which increases the design flow to 1254 cfs just upstream of the culverts that pass under B Street.

As-built plans and topographic information provided by the City of Encinitas and an additional site visit conducted on March 30, 2003, were used to determine existing hydraulic parameters for the storm drain facilities west of Pacific Coast Highway (PCH). Figure 1 illustrates the various channels and structures along this reach of Cottonwood Creek.

Based on topographic information provided by the City of Encinitas, we assumed a slope of 1.5% for the natural channel sections in the study reach. From our site visit, we determined that the channel roughness coefficients ranged from 0.03 to 0.05. Natural channels designated A, B, and D on Figure 1 all have the capacity to convey the design discharge value within their banks. However, natural channel C, located near the entrance to the 10' x 4' RCB and the triple 6'-8" x 5' CMPA flows at a depth of 7.4 feet. This is approximately 2.4 feet above the right overbank. Channel capacity has been constricted by the deposition of sediment caused by backwater from the downstream culverts. The velocities in all of the natural channels range in value from 7.9 fps to 12.3 fps (see Table 2). These high velocities will erode the channel and overbanks, in addition to uprooting smaller trees. To maintain the integrity of the channel and reduce velocities, two solutions have been proposed in Section 3.2.

Our evaluation of the 6' x 4' double box culvert under Third Street showed that the design discharge of 1164 cfs could theoretically reach a depth of 21.7 feet, approximately 13.7 feet above the headwall. In Section 3.2, alternatives to this culvert are discussed.

Downstream from the 6' x 4' double box culvert, there are two sets of culverts, a 10' x 4' RCB and a triple 6'-8" x 5' CMPA, that pass under B Street. To determine the discharge captured by the 10' x 4' RCB near Fourth Street, we determined the maximum amount of flow that enters the triple 6'-8" x 5' CMPA without spilling over the headwall. This value was estimated to be 750 cfs, with the remaining 504 cfs captured by the 10' x 4' RCB. Using this discharge value and a slope of 1.5%, the depth of flow at the upstream end of the 10' x 4' RCB is 8.2 feet. This is

approximately 2.2 feet above the headwall. Alternatives to prevent flooding at this location are discussed in Section 3.2.

Lastly, we looked at the 60-inch and 48-inch RCPs that discharge into the ocean. Based on a slope of 1.5% and a flow value of 504 cfs, we determined that the depth of flow is approximately 8.2 feet. This is roughly 3 feet above the top of the 60-inch pipe. Alternatives to these RCPs are discussed in the next section.

See Table 2 and Appendix A and B for a summary of the existing hydraulic conditions.

3.2 Proposed Alternatives

Natural Channel Sections

Sediment deposition and high velocities are eroding the channel and reducing its ability to convey the design discharge. The following two solutions propose to alleviate these problems:

Solution A: With a regular maintenance program, channel section C should be restored to the dimensions similar to those that are present upstream in channel section B. It would then be able to adequately handle the design flow.

Solution B: One alternative to reduce the velocities (7.9 fps to 12.3 fps) and protect the channel would be to construct drop structures or grade control structures at several locations along the creek.

Third Street Crossing

Three alternatives to the 6' x 4' double box culvert under Third Street were evaluated to convey 1164 cfs at a slope of 2.4%. The alternatives are listed below and are summarized in Table 3. Hydraulic calculations for these alternatives can be found in Appendix C.

Alternative A: 3-7' x 5' RCB with 3' headwall

Alternative B: 2-6' x 4' RCB and 1-10' x 4' RCB

Alternative C: 24' x 6' Conspan Bridge

B Street Crossing

We determined the values of the flow split using different criteria than under the existing conditions. We limited the headwater elevation at the triple 6'-8" x 5' CMPA to the top of the culvert (ignoring the headwall). Under this assumption, the flow entering the culvert would be approximately 580 cfs. The remaining 674 cfs would then enter the existing 10' x 4' RCB.

Two alternatives to the 10' x 4' RCB that pass under B Street were proposed to convey 674 cfs at a slope of 1.5%. The alternatives are listed below and are summarized in Table 3. Hydraulic calculations for these alternatives can be found in Appendix C.

Alternative A: 3-10' x 4' RCB with 2' headwall

Alternative B: 20' x 5' Conspan Bridge

Ocean Outfall

Three alternatives to the 60-inch and 48-inch RCPs that convey 580 cfs to the ocean under the volleyball courts were proposed. The alternatives are listed below and are summarized in Table 3. Hydraulic calculations for these alternatives can be found in Appendix C.

Alternative A: 3-6' x 5' RCB with 1.5' headwall

Alternative B: 16' x 5' Conspan Bridge

Alternative C: 2- 60" RCP and 48" RCP

3.3 Proposed Fourth Street Storm Drain System

During a significant storm event, runoff has historically ponded at the intersection of Fourth Street and A Street before cascading southerly down Fourth Street to Cottonwood Creek. This area has become a safety hazard due to the quantity and velocity of the water as it sheet flows down Fourth Street. One alternative that has been discussed with the City is to construct several curb inlets along Fourth Street immediately south of its intersection with A Street (just before runoff is conveyed down the hill). Using our Rational Method study, we determined that the contributing flow to this point from all upstream areas is approximately 100 cfs. We have sized the inlets assuming 100% capture. If each inlet captures 50 cfs, two 65-foot inlets are needed.

Assuming a slope of 11.3%, a 36-inch storm drain pipe is required to convey 100 cfs. A length has not been specified due to the unknown tie-in location.

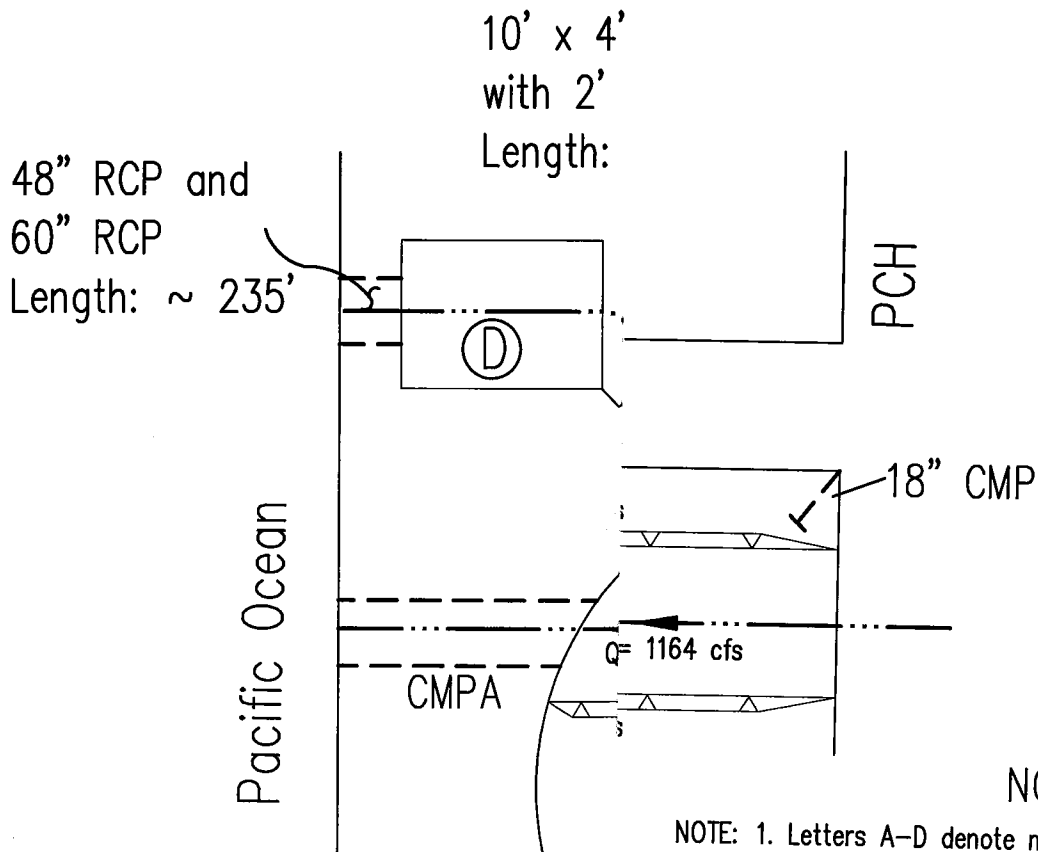
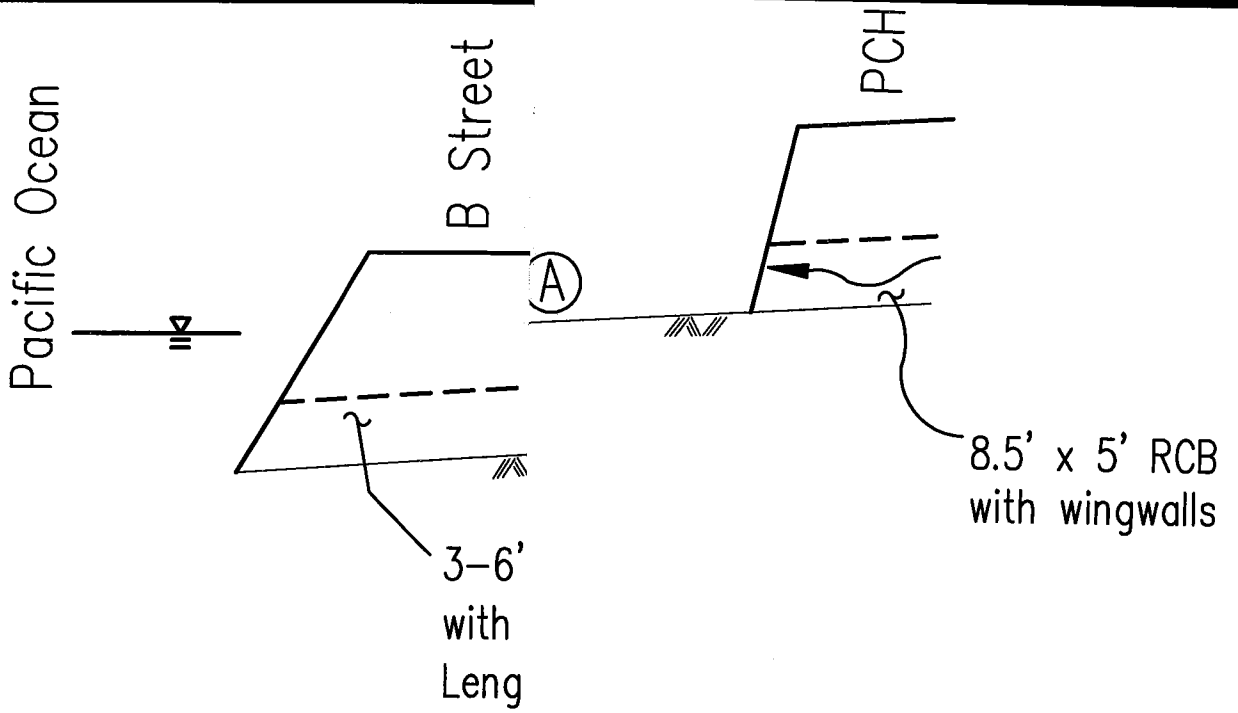
Hydraulic calculations for this analysis can be found in Appendix D.

Table 2: Existing Conditions Cottonwood Creek

Location		Headwater Elevation (ft)	Depth (ft)
Between PCH and 3rd St.	A: ~ 35'	N/A	5.21
3rd St. Culvert Crossing	Dou	21.7	N/A
Between 3rd St. and 4th St.	B: 25' x	N/A	3.77
Between 3rd St. and Triple CMPA entrance	C: Irregu	N/A	7.40
Southern Ocean Outfall	Triple	6.11	N/A
B St. Culvert Crossing		8.24	N/A
Between B St. and Ocean Outfall	D: 10' x	N/A	4.63
Northern Ocean Outfall	60" F	8.23	N/A

Table 3: Proposed Alternatives Cottonwood Creek

Location	
3rd St. Culvert Crossing	Alt.A: 3-7' x 5' RCB w
	Alt. B: 2-6' x 4' RCB a
	Alt. C: 24' x 6' Conspa
B St. Culvert Crossing	Alt. A: 3-10' x 4' RCB
	Alt. B: 20' x 5' Conspa
Northern Ocean Outfall	Alt. A: 3-6' x 5' RCB v
	Alt. B: 16' x 5' Conspa
	Alt. C: 2- 60" RCP and



- NOTE: 1. Letters A-D denote natural channel sections. Refer to Appendices for hydraulic information.
2. Hydraulic information about existing and proposed storm drain structures is found in the Appendix.

XREFS: X11X17L

DATE: 04/10/03 TIME: 8:46 a.m.
 SERVER: NONE SERVICE: NONE
 PATH: N:\sd0948\Cadd\
 DRAWING NAME: COTTONWOOD CR. SCHEMATIC.DWG
 PLOTTING VIEW: NONE
 DESIGNER: NONE PROJ. MGR: JWG

ht Beach
 lities

SHEET NUMBER

1

OF 1 SHEETS

DATE SUBMITTED: 04/09/03

JOB NUMBER
 SD094800

APPENDIX A
EXISTING CONDITIONS: NATURAL CHANNEL HYDRAULIC CALCULATIONS

COTTONWOOD CREEK/MOONLIGHT BEACH

Hydrology and Facilities Analysis Summary

Natural Channel A: ~ 35'x 6'

Irregular Channel A

Worksheet for Irregular Channel

Project Description

Worksheet	Irregular Channel
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Slope	0.15000 ft/ft
Discharge	164.00 cfs

Options

Current Roughness Method	used Lotter's Method
Open Channel Weighting	used Lotter's Method
Closed Channel Weighting	Horton's Method

Results

Mannings Coefficient	0.050
Water Surface Elev.	5.21 ft
Elevation Range	0.00 to 7.00
Flow Area	141.8 ft ²
Wetted Perimeter	41.87 ft
Top Width	33.80 ft
Actual Depth	5.21 ft
Critical Elevation	4.31 ft
Critical Slope	0.031130 ft/ft
Velocity	8.21 ft/s
Velocity Head	1.05 ft
Specific Energy	6.25 ft
Froude Number	0.71
Flow Type	Subcritical

Roughness Segments

Start Station	End Station	Mannings Coefficient
0+00	0+35	0.050

Natural Channel Points

Station (ft)	Elevation (ft)
0+00	7.00
0+02	1.00
0+15	1.00
0+15	0.00
0+20	0.00
0+20	1.00
0+33	1.00
0+35	7.00

Natural Channel B: 25' x 6.5'

Rectangular Channel B

Worksheet for Rectangular Channel

Project Description

Worksheet	Rectangular Chan
Flow Element	Rectangular Chan
Method	Manning's Formul
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.030
Slope	015000 ft/ft
Bottom Width	25.00 ft
Discharge	,164.00 cfs

Results

Depth	3.77 ft
Flow Area	94.4 ft ²
Wetted Perimx	32.55 ft
Top Width	25.00 ft
Critical Depth	4.07 ft
Critical Slope	0.011961 ft/ft
Velocity	12.33 ft/s
Velocity Head	2.36 ft
Specific Enerç	6.14 ft
Froude Numbx	1.12
Flow Type	supercritical

Natural Channel C: Irregular

Irregular Rectangular Channel C Worksheet for Irregular Channel

Project Description

Worksheet	Irregular Channel
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Slope	0.15000 ft/ft
Discharge	164.00 cfs

Options

Current Roughness Method	Selected	Lotter's Method
Open Channel Weighting	Selected	Lotter's Method
Closed Channel Weighting	Selected	Horton's Method

Results

Manning's Coefficient	0.047
Water Surface Elev.	7.40 ft
Elevation Range	.00 to 8.00
Flow Area	147.3 ft ²
Wetted Perimeter	50.98 ft
Top Width	38.00 ft
Actual Depth	7.40 ft
Critical Elevation	6.60 ft
Critical Slope	0.030998 ft/ft
Velocity	7.90 ft/s
Velocity Head	0.97 ft
Specific Energy	8.37 ft
Froude Number	0.71
Flow Type	Subcritical

Calculation Messages:

Water elevation exceeds lowest end station by 2.4022296 ft.

Roughness Segments

Start Station	End Station	Manning's Coefficient
0+00	0+20	0.050
0+20	0+27	0.040
0+27	0+38	0.050

Natural Channel Points

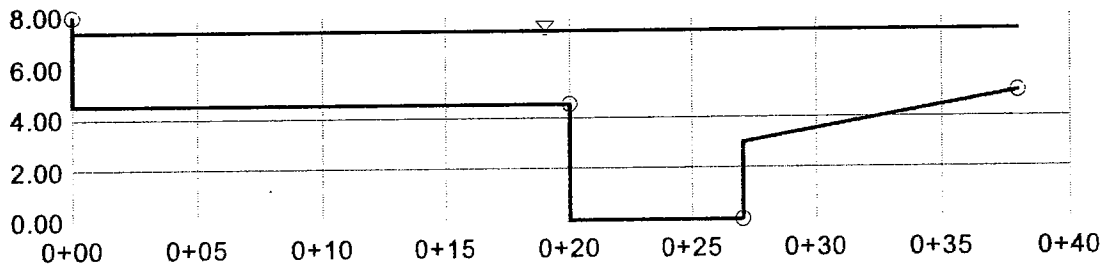
Station (ft)	Elevation (ft)
0+00	8.00
0+00	4.50
0+20	4.50
0+20	0.00
0+27	0.00
0+27	3.00
0+38	5.00

Cross Section

Cross Section for Irregular Channel

Project Description	
Worksheet	Irregular Channel
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.047
Slope	0.015000 ft/ft
Water Surface Elev.	7.40 ft
Elevation Range	.00 to 8.00
Discharge	1,164.00 cfs



V:1
H:1
NTS

COTTONWOOD CREEK/MOONLIGHT BEACH

Hydrology and Facilities Analysis Summary

Natural Channel D: 10' x 5.5'

Rectangular Channel D

Worksheet for Rectangular Channel

Project Description

Worksheet	Rectangular Chan
Flow Element	Rectangular Chan
Method	Manning's Formul
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.030
Slope	015000 ft/ft
Bottom Width	10.00 ft
Discharge	504.00 cfs

Results

Depth	4.63 ft
Flow Area	46.3 ft ²
Wetted Perim	19.26 ft
Top Width	10.00 ft
Critical Depth	4.29 ft
Critical Slope	0.018436 ft/ft
Velocity	10.89 ft/s
Velocity Head	1.84 ft
Specific Energ	6.47 ft
Froude Numb	0.89
Flow Type	Subcritical

APPENDIX B

EXISTING CONDITIONS: STORM DRAIN FACILITIES CALCULATIONS

Third Street Culvert Crossing

Double 6' x 4' RCB

Culvert Calculator Report 6x4 Double Box Culvert (Existing)

Solve For: Headwater Elevation

Culvert Summary

Allowable HW Elevation	24.15 ft	Headwater Depth/Height	5.42
Computed Headwater Elev.	37.85 ft	Discharge	1,164.00 cfs
Inlet Control HW Elev.	37.85 ft	Tailwater Elevation	17.81 ft
Outlet Control HW Elev.	33.14 ft	Control Type	Inlet Control

Grades

Upstream Invert	16.15 ft	Downstream Invert	14.04 ft
Length	88.00 ft	Constructed Slope	0.023977 ft/ft

Hydraulic Profile

Profile	PressureProfile	Depth, Downstream	4.00 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	4.00 ft
Velocity Downstream	24.25 ft/s	Critical Slope	0.046994 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.015
Section Material	Concrete	Span	6.00 ft
Section Size	6 x 4 ft	Rise	4.00 ft
Number Sections	2		

Outlet Control Properties

Outlet Control HW Elev.	33.14 ft	Upstream Velocity Head	9.14 ft
Ke	0.20	Entrance Loss	1.83 ft

Inlet Control Properties

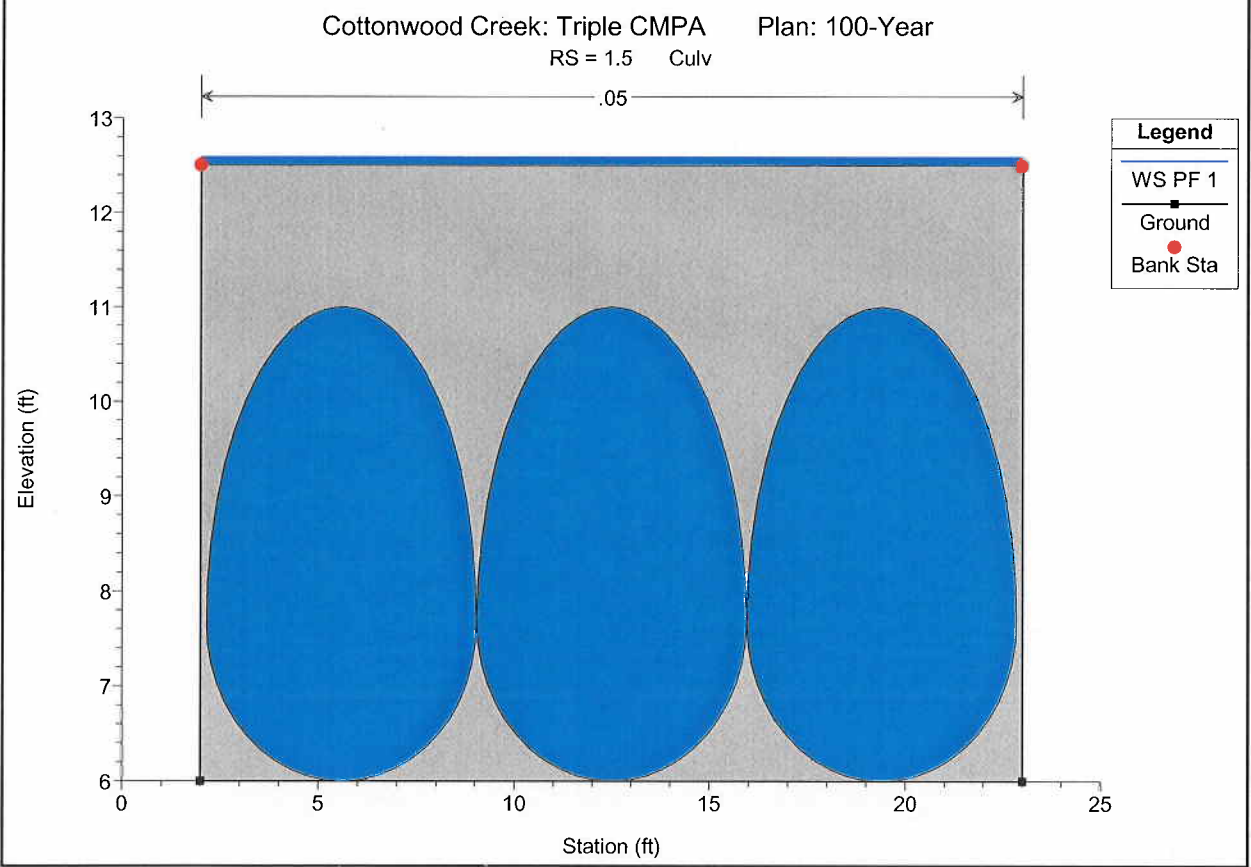
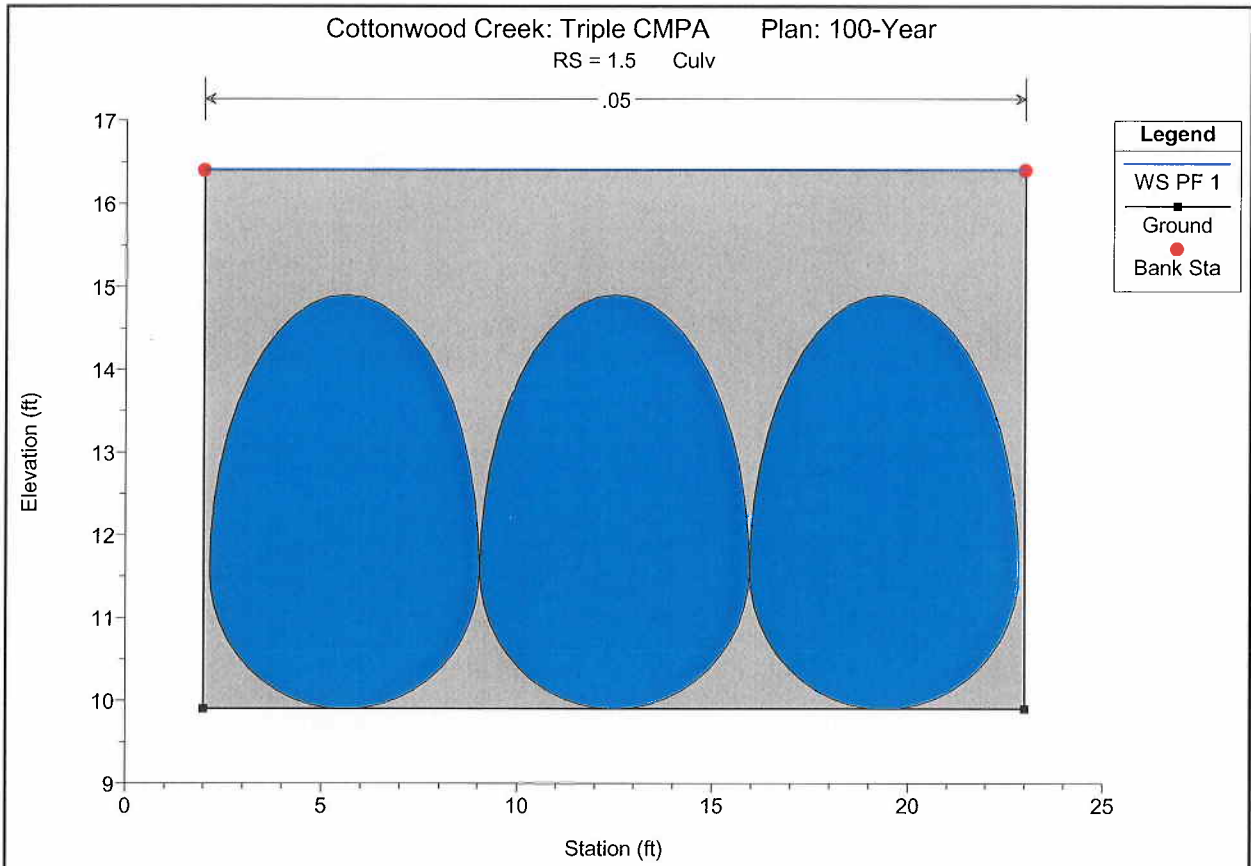
Inlet Control HW Elev.	37.85 ft	Flow Control	N/A
Inlet Type	90° headwall w 45° bevels	Area Full	48.0 ft ²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

Southern Ocean Outfall

Triple 6'-8" x 5' CMPA

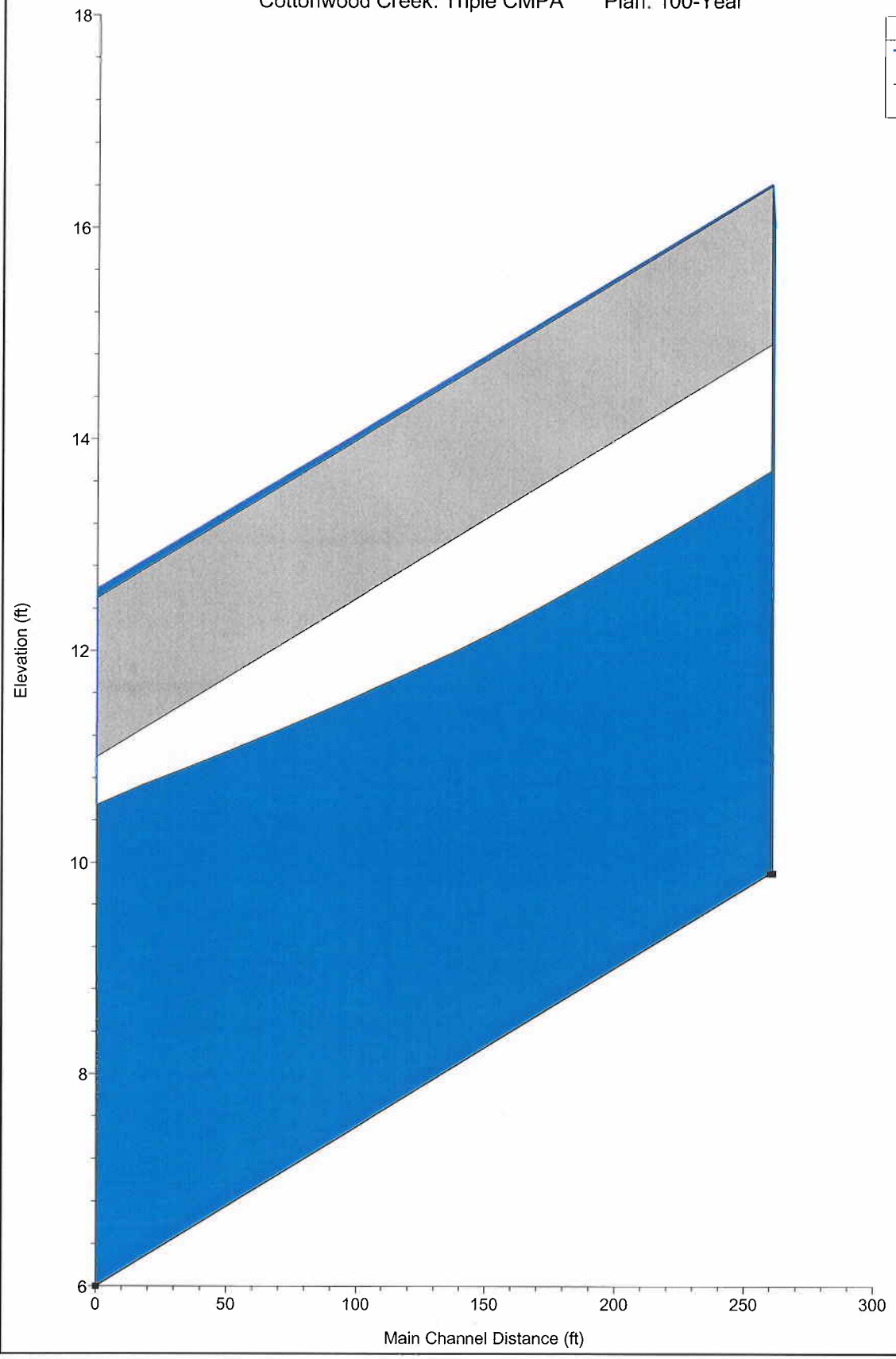
HEC-RAS Plan: 100-Year River: Cottonwood Creek Reach: Ocean Outfall Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E. G. Elev (ft)	E. G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Ocean Outfall	2	PF 1	750.00	9.90	16.01	13.30	16.54	0.006398	5.85	128.21	21.00	0.42
Ocean Outfall	1.5	Culvert										
Ocean Outfall	1	PF 1	750.00	6.00	10.54	9.40	11.50	0.015003	7.86	95.44	21.00	0.65



Cottonwood Creek: Triple CMPA Plan: 100-Year

Legend	
WS PF 1	—
Ground	■



B Street Culvert Crossing

10'x4' RCB

Culvert Calculator Report

10x4 Box Culvert (Existing)

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	15.00 ft	Headwater Depth/Height	2.06
Computed Headwater Elev:	17.24 ft	Discharge	504.00 cfs
Inlet Control HW Elev.	17.24 ft	Tailwater Elevation	13.63 ft
Outlet Control HW Elev.	17.19 ft	Control Type	Inlet Control

Grades			
Upstream Invert	9.00 ft	Downstream Invert	8.10 ft
Length	60.00 ft	Constructed Slope	0.015000 ft/ft

Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	3.34 ft
Slope Type	N/A	Normal Depth	2.81 ft
Flow Regime	N/A	Critical Depth	4.00 ft
Velocity Downstream	15.10 ft/s	Critical Slope	0.010055 ft/ft

Section			
Section Shape	Box	Mannings Coefficient	0.015
Section Material	Concrete	Span	10.00 ft
Section Size	10 x 4 ft	Rise	4.00 ft
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	17.19 ft	Upstream Velocity Head	2.47 ft
Ke	0.20	Entrance Loss	0.49 ft

Inlet Control Properties			
Inlet Control HW Elev.	17.24 ft	Flow Control	N/A
Inlet Type	90° headwall w 45° bevels	Area Full	40.0 ft ²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

Northern Ocean Outfall

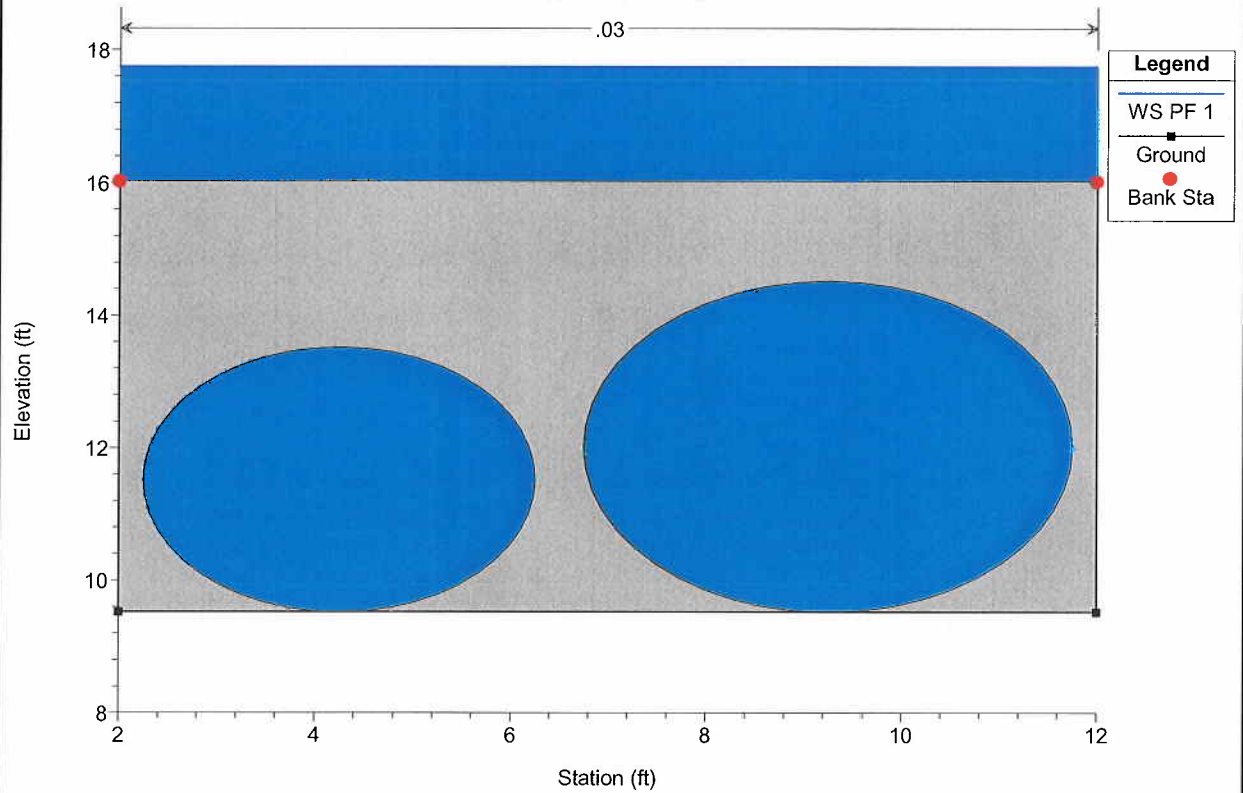
60" RCP and 48" RCP

HEC-RAS Plan: 100-Year River: Cottonwood Creek Reach: Beach Outfall Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev. (ft)	Crit W.S. (ft)	E.G. Elev. (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Beach Outfall	2	PF 1	504.00	9.52	17.75	13.80	18.33	0.003367	6.12	82.29	10.00	0.38
Beach Outfall	1.5	Culvert										
Beach Outfall	1	PF 1	504.00	6.00	10.63	10.27	12.47	0.015001	10.89	46.30	10.00	0.89

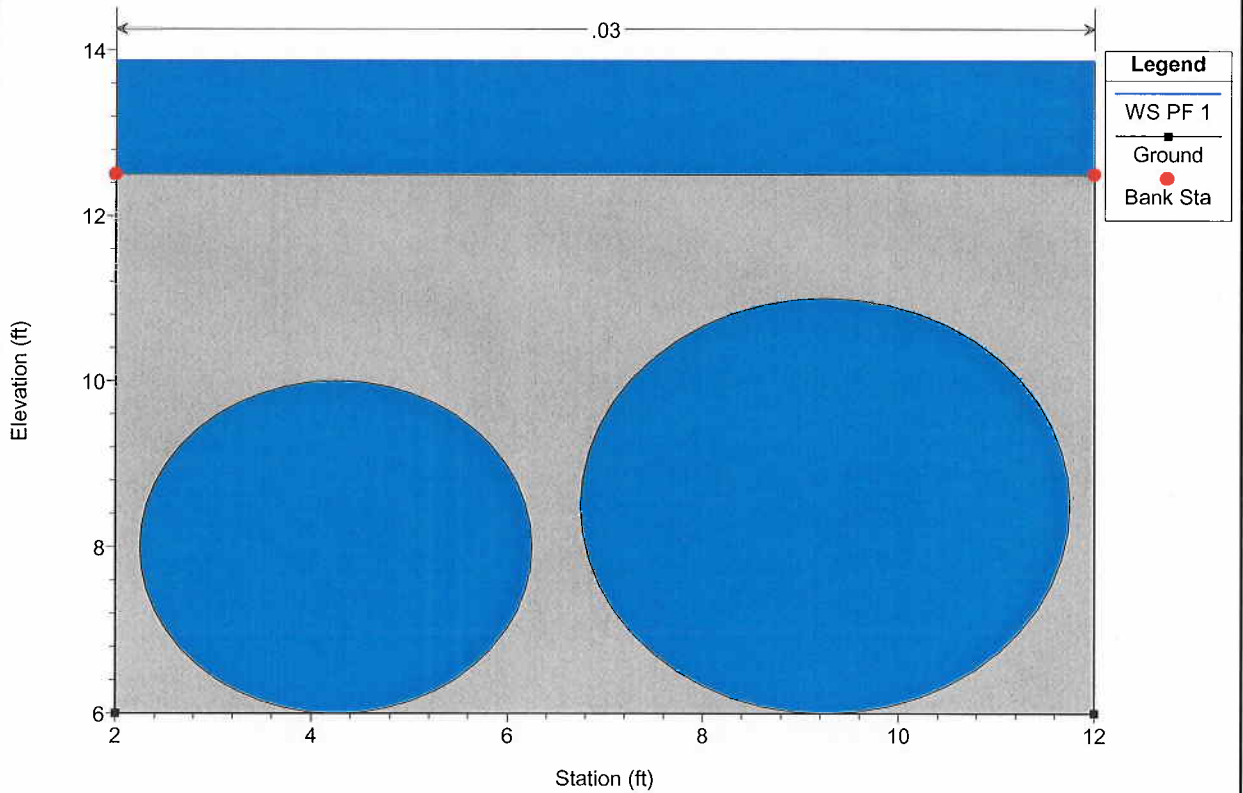
Cottonwood Creek: 48" and 60" RCP Plan: 100-Year

RS = 1.5 Culv

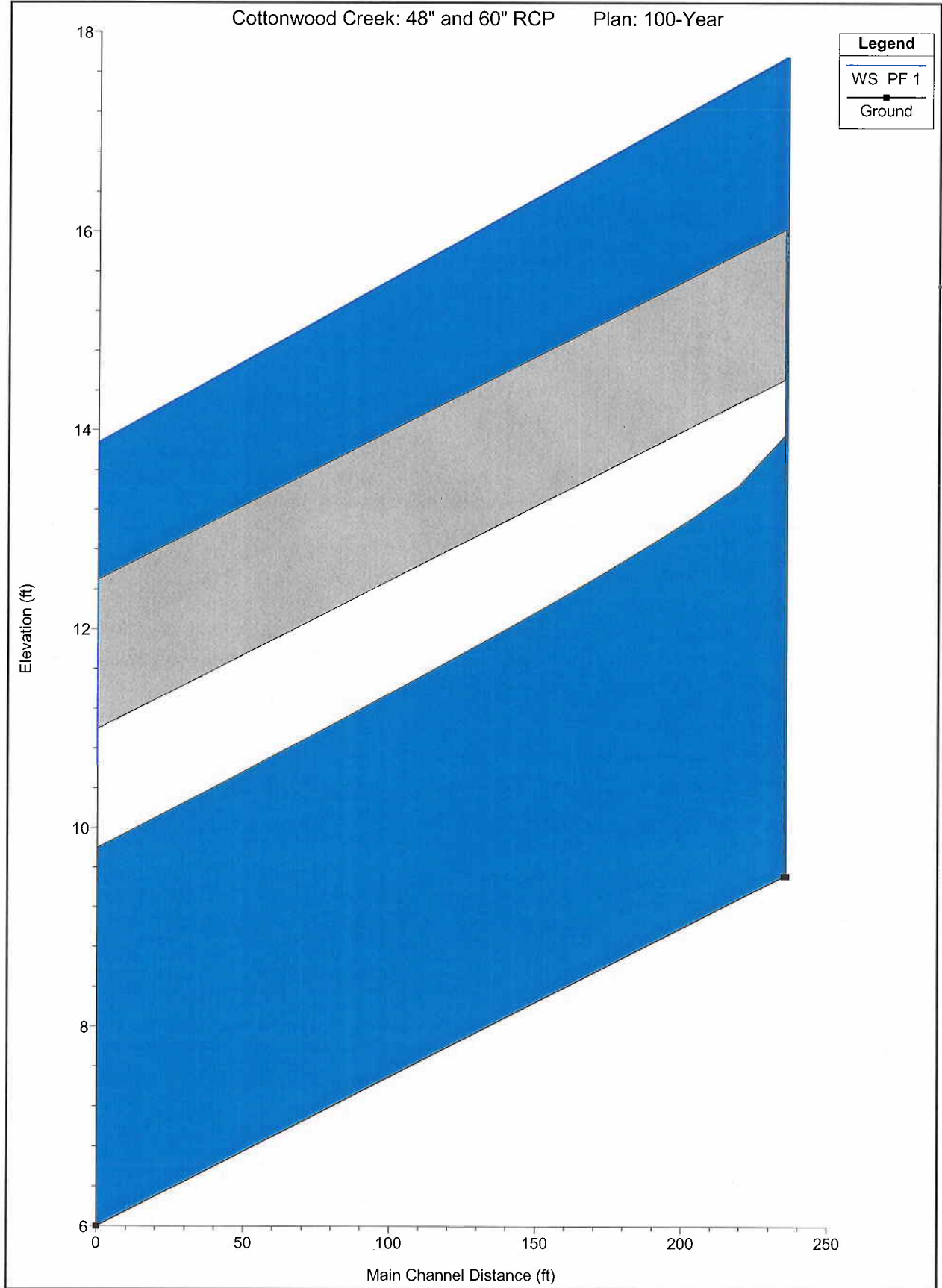


Cottonwood Creek: 48" and 60" RCP Plan: 100-Year

RS = 1.5 Culv



Cottonwood Creek: 48" and 60" RCP Plan: 100-Year



APPENDIX C

PROPOSED ALTERNATIVES: STORM DRAIN FACILITIES CALCULATIONS

Third Street Culvert Crossing

- Alternative A: 3-7' x 5' RCB w/ 3' headwall
- Alternative B: 2-6' x 4' RCB and 1-10' x 4' RCB
- Alternative C: 24' x 6' Conspan Bridge

COTTONWOOD CREEK/MOONLIGHT BEACH

Hydrology and Facilities Analysis Summary

Alternative A: 3-7' x 5' RCB w/ 3' headwall

Culvert Calculator Report Alternative A

Solve For: Headwater Elevation

Culvert Summary

Allowable HW Elevation	24.15 ft	Headwater Depth/Height	1.58
Computed Headwater Elev.	24.05 ft	Discharge	1,164.00 cfs
Inlet Control HW Elev.	24.05 ft	Tailwater Elevation	17.81 ft
Outlet Control HW Elev.	23.46 ft	Control Type	Inlet Control

Grades

Upstream Invert	16.15 ft	Downstream Invert	14.04 ft
Length	88.00 ft	Constructed Slope	0.023977 ft/ft

Hydraulic Profile

Profile	S2	Depth, Downstream	3.18 ft
Slope Type	Steep	Normal Depth	2.72 ft
Flow Regime	Supercritical	Critical Depth	4.57 ft
Velocity Downstream	17.42 ft/s	Critical Slope	0.006019 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.015
Section Material	Concrete	Span	7.00 ft
Section Size	7 x 5 ft	Rise	5.00 ft
Number Sections	3		

Outlet Control Properties

Outlet Control HW Elev.	23.46 ft	Upstream Velocity Head	2.29 ft
Ke	0.20	Entrance Loss	0.46 ft

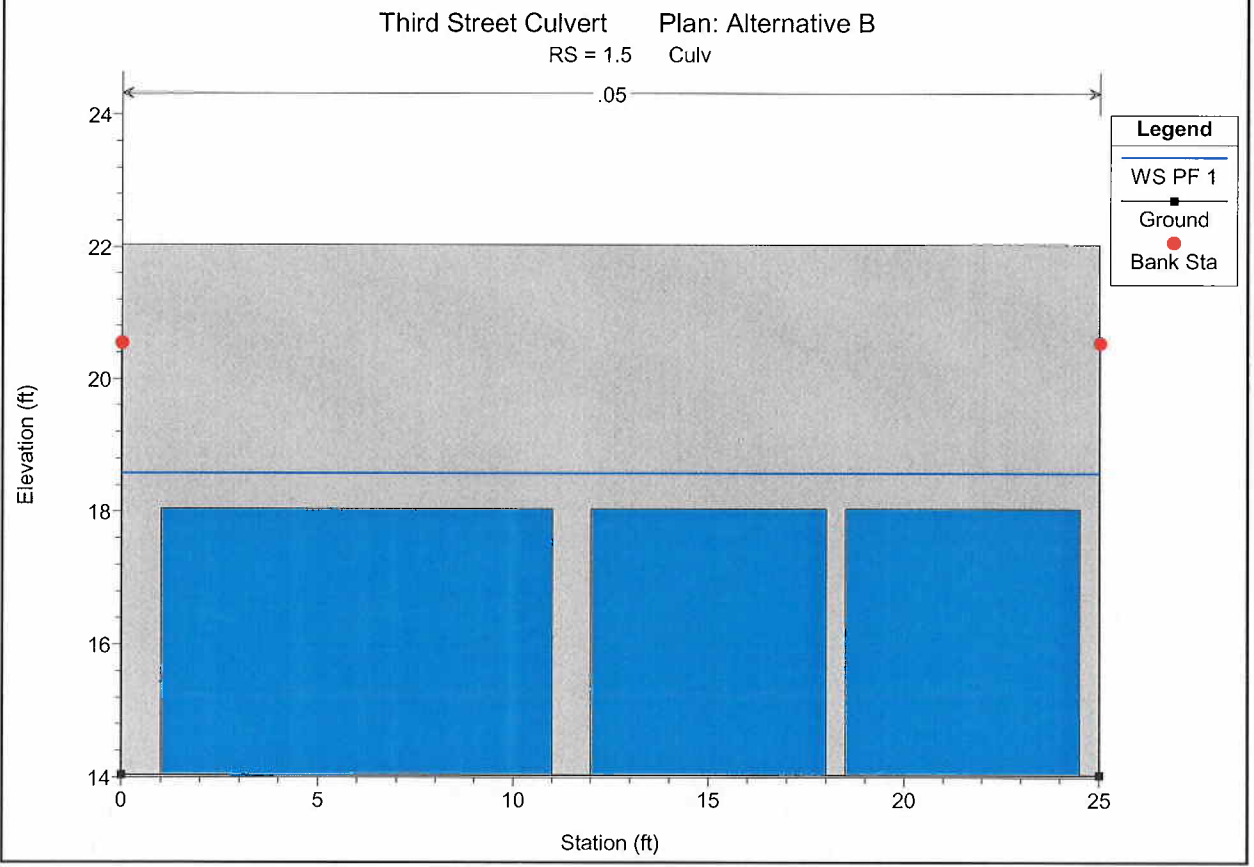
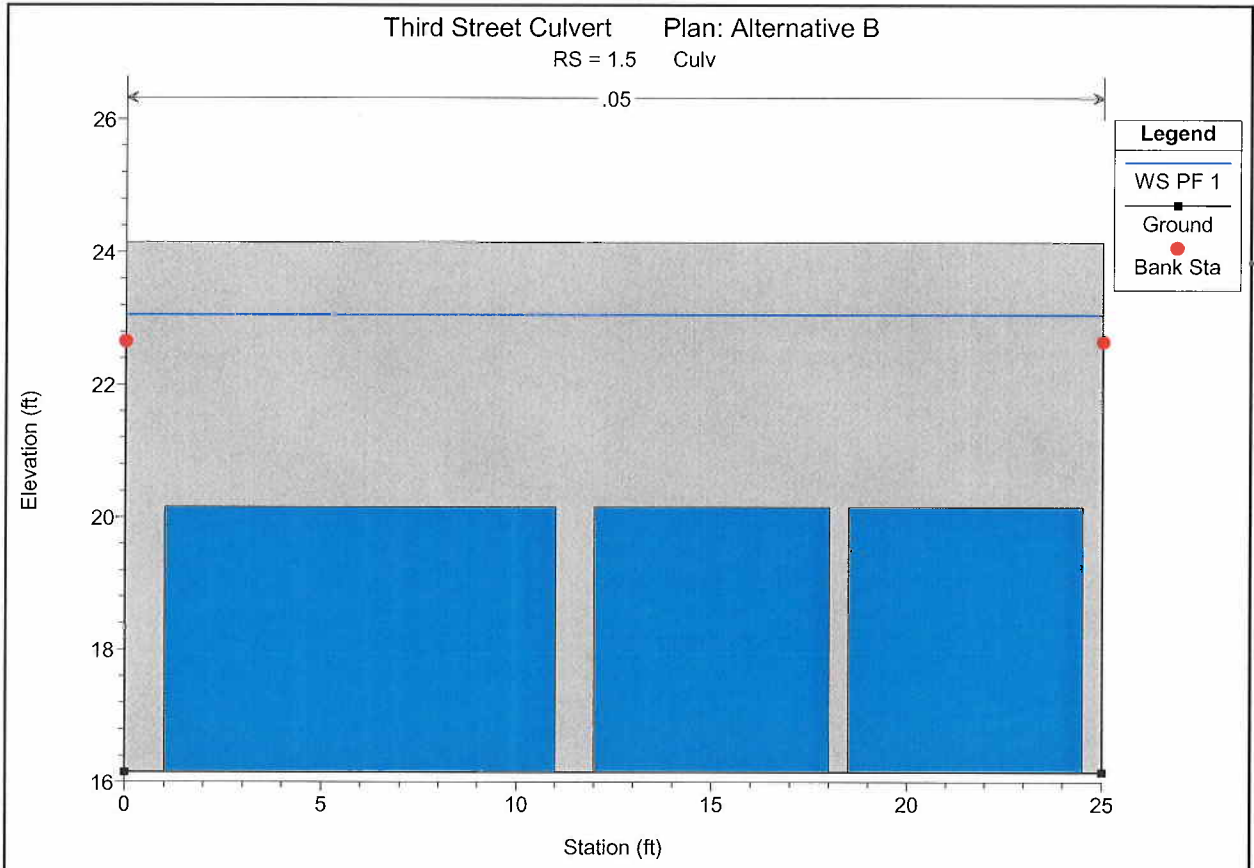
Inlet Control Properties

Inlet Control HW Elev.	24.05 ft	Flow Control	Submerged
Inlet Type	90° headwall w 45° bevels	Area Full	105.0 ft²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

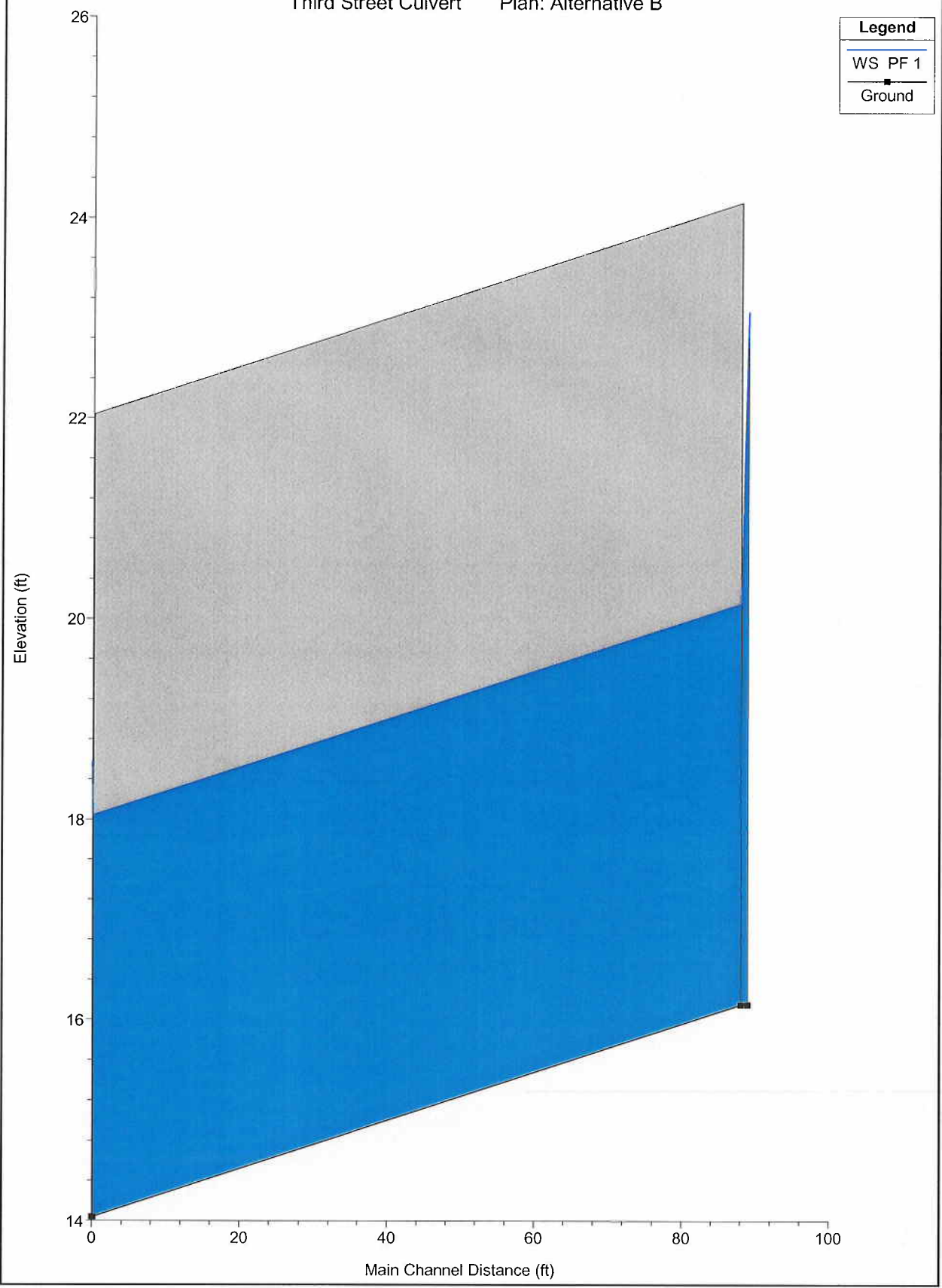
Alternative B: 2-6' x 4' RCB and 1-10' x 4' RCB

HEC-RAS Plan: 100-Year River: Cottonwood Creek Reach: Third Street Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Third Street	2	PF 1	1164.00	16.15	23.06	20.22	23.76	0.007031	6.74	172.68	25.00	0.45
Third Street	1.5	Culvert										
Third Street	1	PF 1	1164.00	14.04	18.58	18.11	20.21	0.024007	10.26	113.40	25.00	0.85



Third Street Culvert Plan: Alternative B

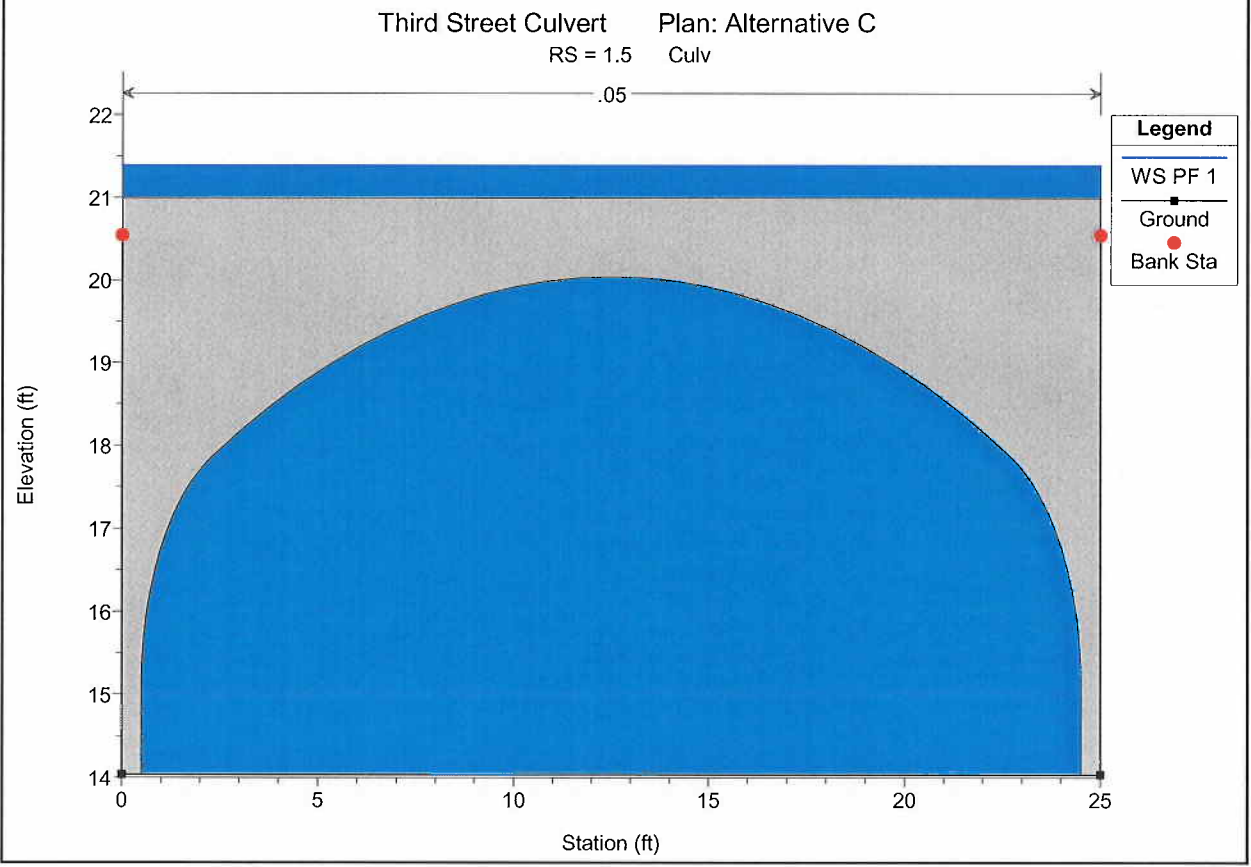
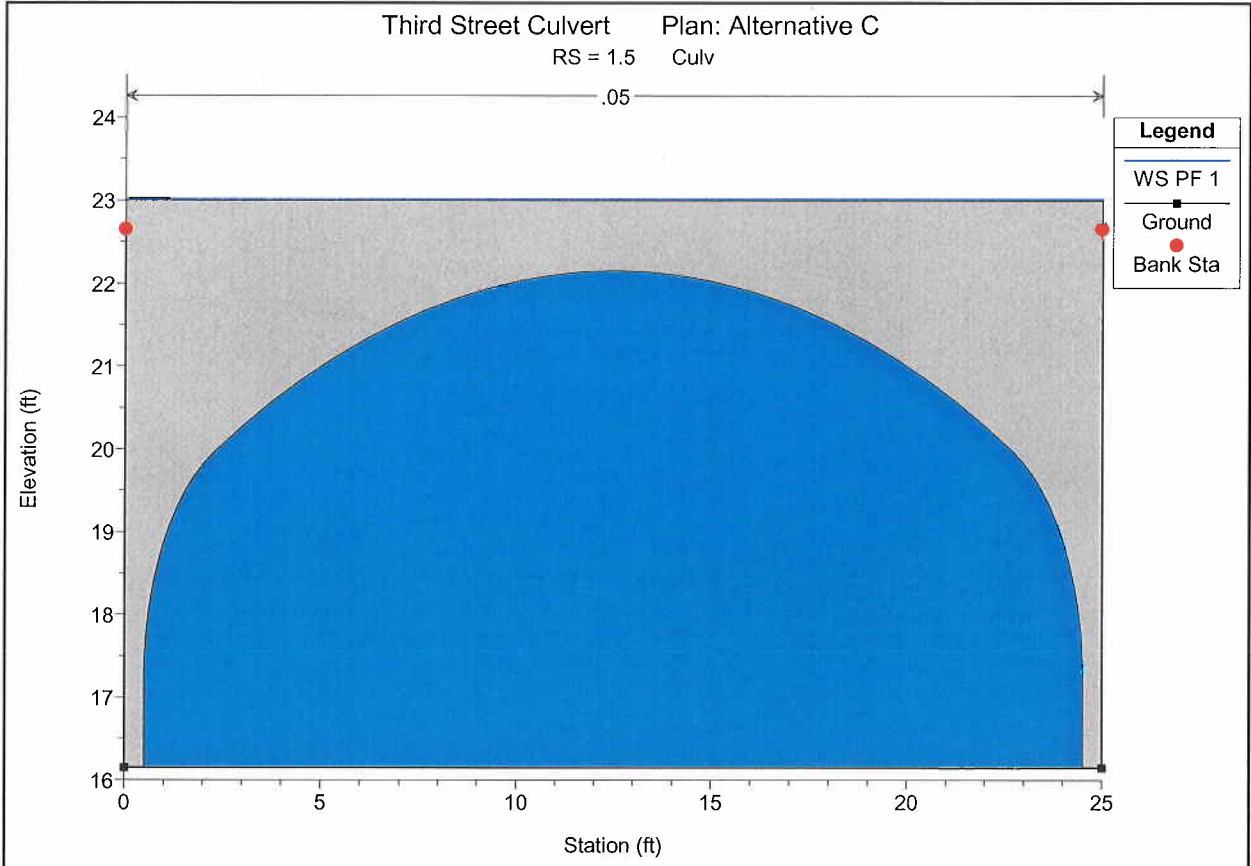


Legend	
—	WS PF 1
■	Ground

Alternative C: 24' x 6' Conspan Bridge

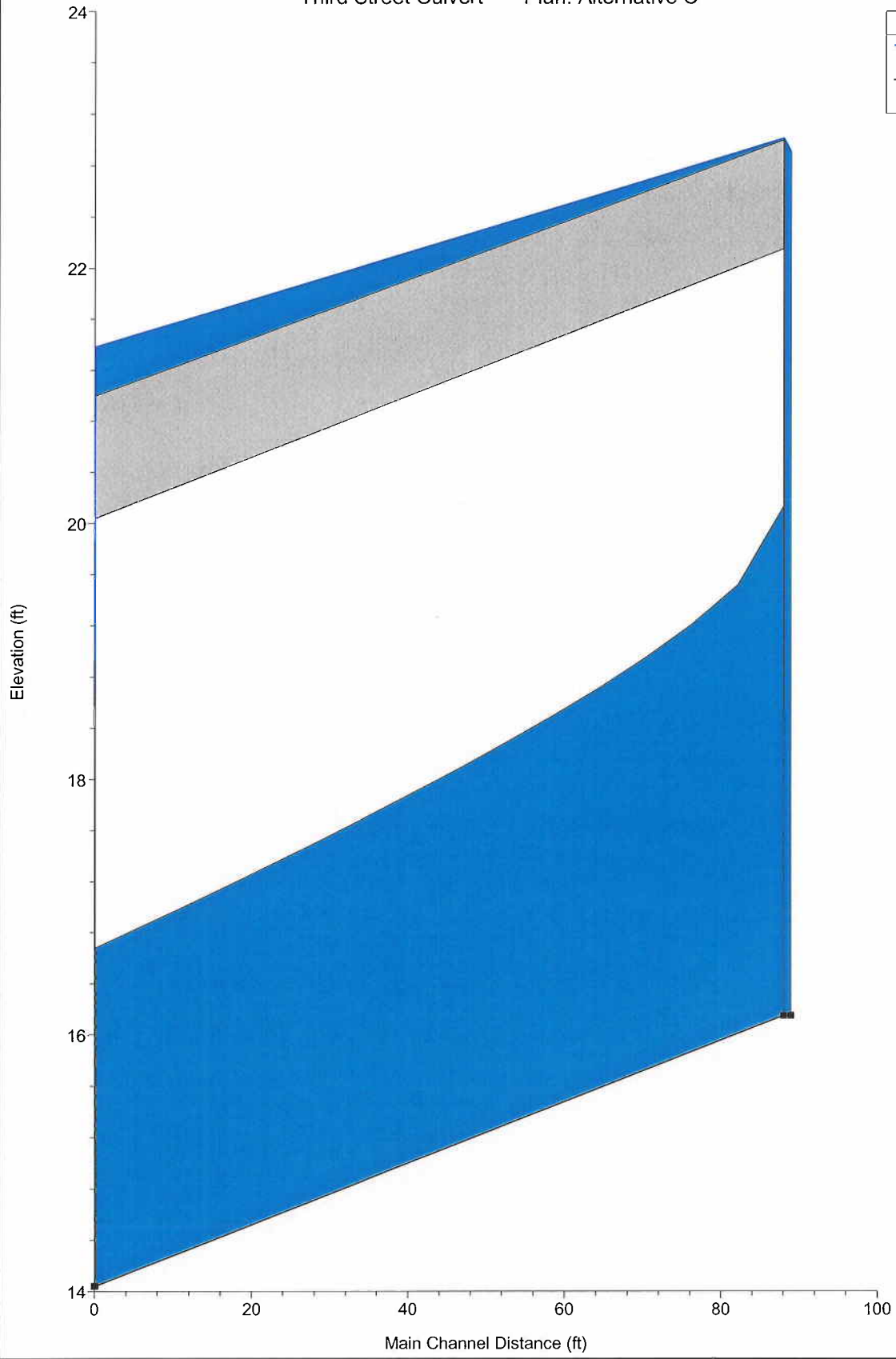
HEC-RAS Plan: 100-Year River: Cottonwood Creek Reach: Third Street Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Third Street	2	PF 1	1164.00	16.15	22.90	20.22	23.64	0.007496	6.89	168.86	25.00	0.47
Third Street	1.5	Culvert										
Third Street	1	PF 1	1164.00	14.04	18.58	18.11	20.21	0.024007	10.26	113.40	25.00	0.85



Third Street Culvert Plan: Alternative C

Legend	
WS PF 1	—
Ground	■



B Street Culvert Crossing

Alternative A: 3-10' x 4' RCB w/ 2' headwall

Alternative B: 20' x 5' Conspan Bridge

COTTONWOOD CREEK/MOONLIGHT BEACH

Hydrology and Facilities Analysis Summary

Alternative A: 3-10' x 4' RCB w/ 2' headwall

Culvert Calculator Report

10x4 Box Culvert Alternative A

Solve For: Headwater Elevation

Culvert Summary

Allowable HW Elevation	15.00 ft	Headwater Depth/Height	1.39
Computed Headwater Elev.	14.57 ft	Discharge	674.00 cfs
Inlet Control HW Elev.	13.86 ft	Tailwater Elevation	13.86 ft
Outlet Control HW Elev.	14.57 ft	Control Type	Outlet Control

Grades

Upstream Invert	9.00 ft	Downstream Invert	8.10 ft
Length	60.00 ft	Constructed Slope	0.015000 ft/ft

Hydraulic Profile

Profile	PressureProfile	Depth, Downstream	5.76 ft
Slope Type	N/A	Normal Depth	1.62 ft
Flow Regime	N/A	Critical Depth	2.50 ft
Velocity Downstream	5.62 ft/s	Critical Slope	0.004149 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.015
Section Material	Concrete	Span	10.00 ft
Section Size	10 x 4 ft	Rise	4.00 ft
Number Sections	3		

Outlet Control Properties

Outlet Control HW Elev.	14.57 ft	Upstream Velocity Head	0.49 ft
Ke	0.20	Entrance Loss	0.10 ft

Inlet Control Properties

Inlet Control HW Elev.	13.86 ft	Flow Control	Unsubmerged
Inlet Type	90° headwall w 45° bevels	Area Full	120.0 ft ²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

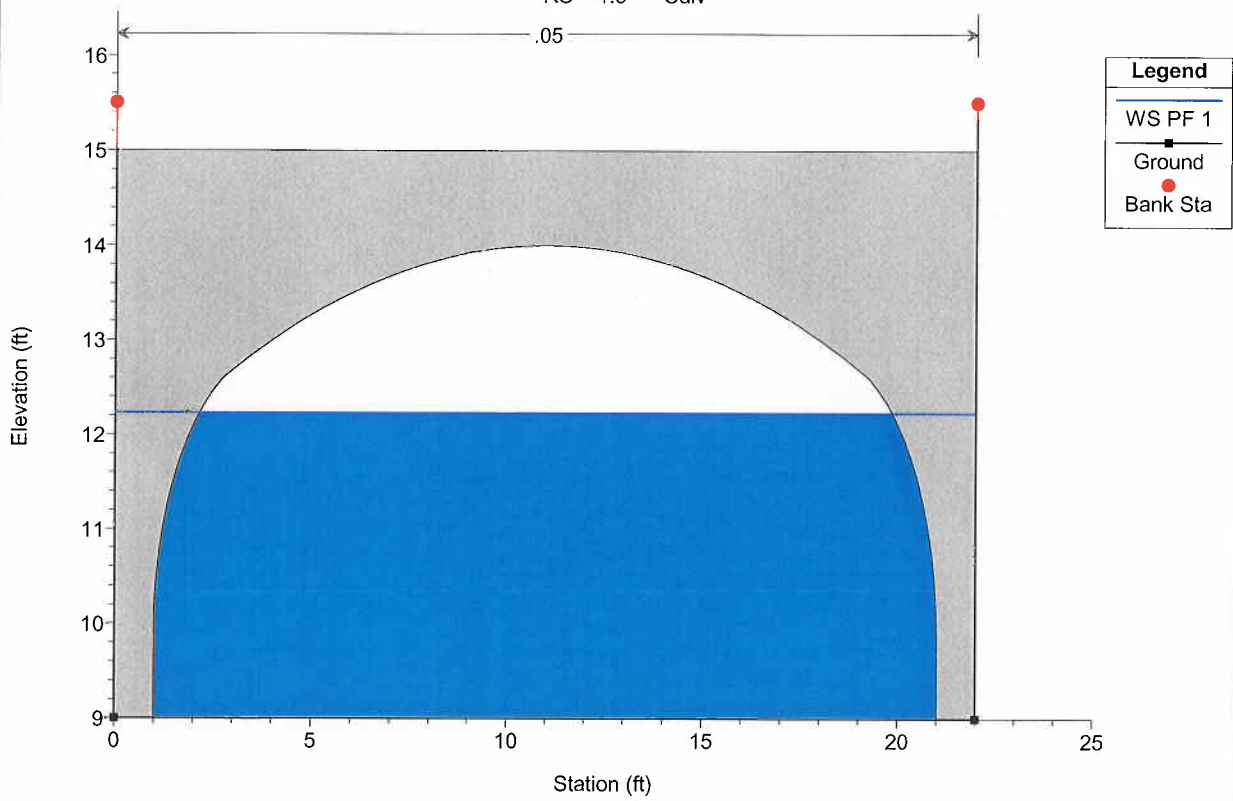
Alternative B: 20' x 5' Conspan Bridge

HEC-RAS Plan: 100-Year River: Cottonwood Creek Reach: B Street Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
B Street	2	PF 1	674.00	9.00	14.40	12.07	14.90	0.006549	5.67	118.82	22.00	0.43
B Street	1.5	Culvert										
B Street	1	PF 1	674.00	8.10	12.17	11.17	13.05	0.015013	7.53	89.56	22.00	0.66

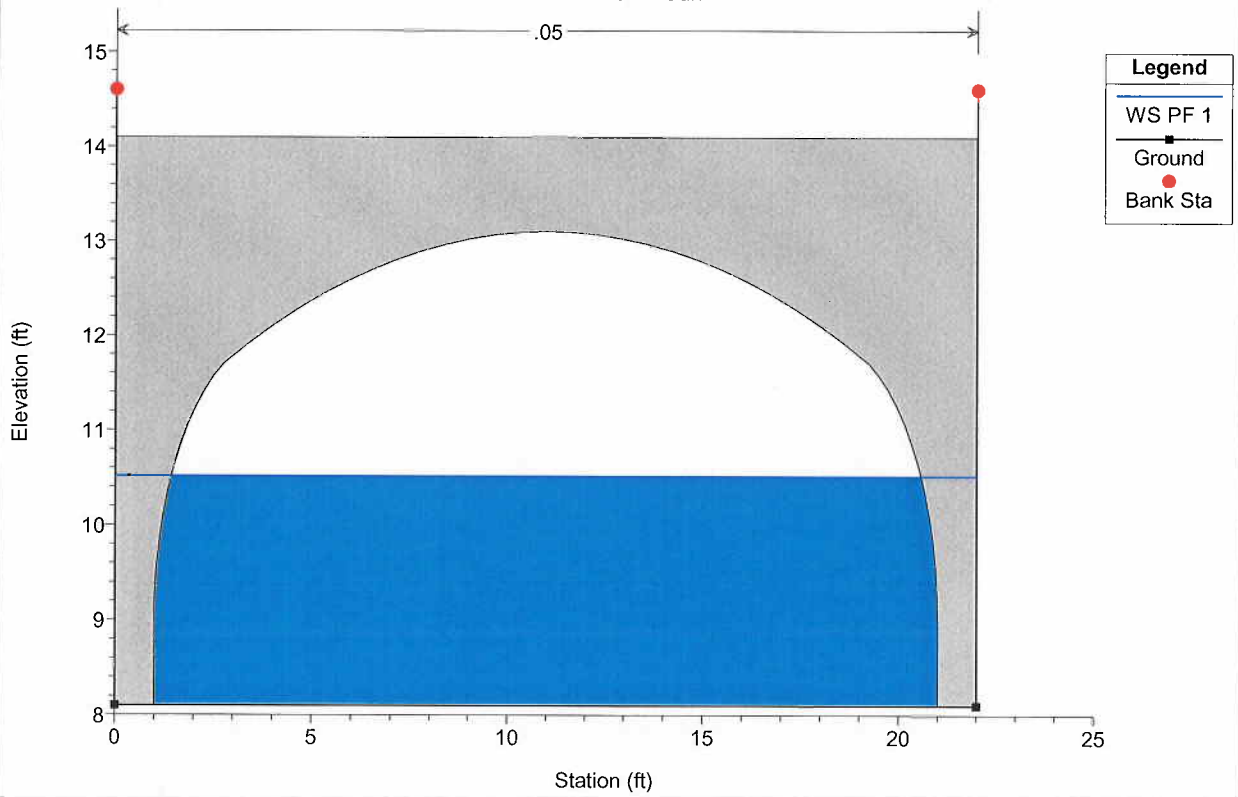
B Street Culvert Crossing Plan: Alternative B

RS = 1.5 Culv

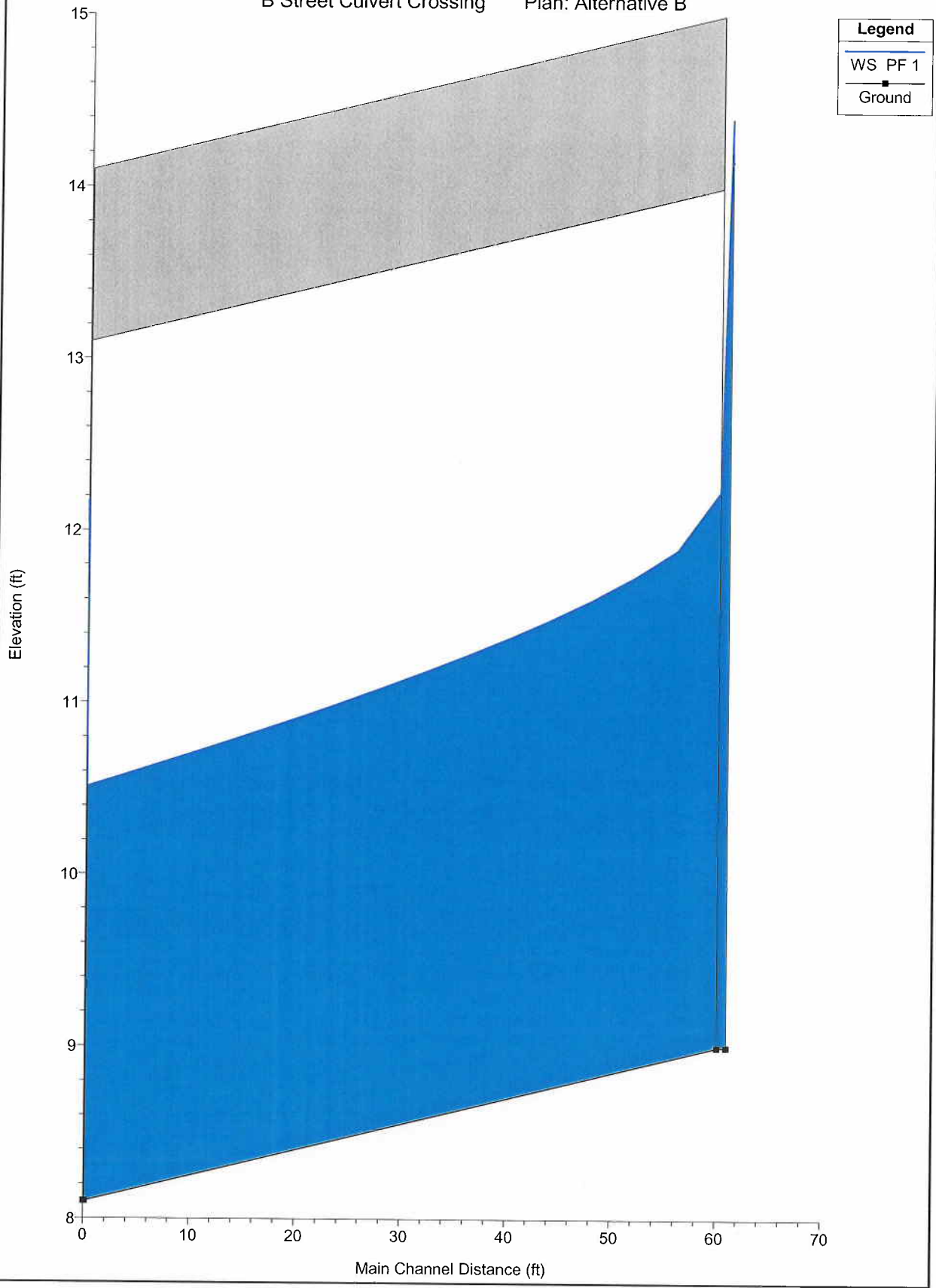


B Street Culvert Crossing Plan: Alternative B

RS = 1.5 Culv



B Street Culvert Crossing Plan: Alternative B



Northern Ocean Outfall

Alternative A: 3-6' x 5' RCB w/ 1.5' headwall

Alternative B: 16' x 5' Conspan Bridge

Alternative C: 2- 60" RCP and 48" RCP

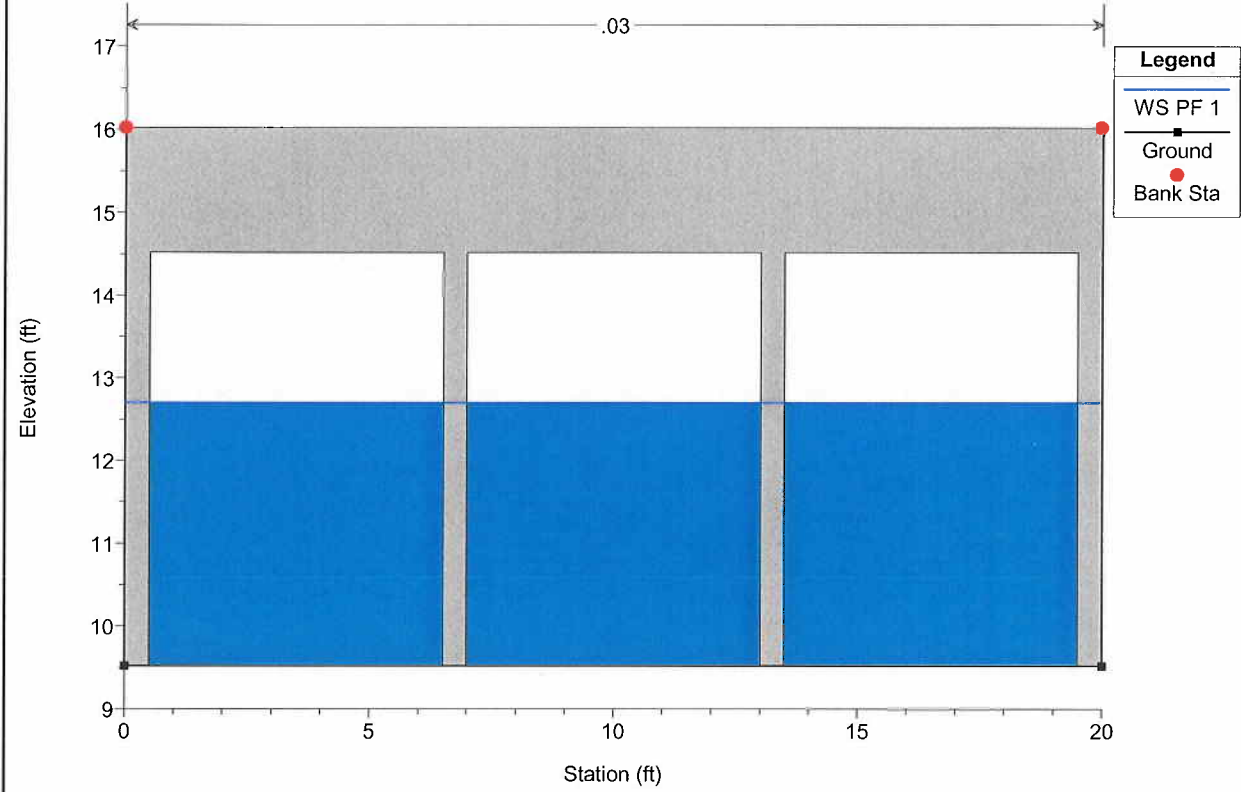
Alternative A: 3-6' x 5' RCB w/ 1.5' headwall

HEC-RAS Plan: 100-Year River: Cottonwood Creek Reach: Ocean Outfall Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Ocean Outfall	2	PF 1	580.00	9.52	14.58	12.48	15.09	0.002661	5.73	101.19	20.00	0.45
Ocean Outfall	1.5	Culvert										
Ocean Outfall	1	PF 1	580.00	6.00	8.96	8.96	10.45	0.013061	9.81	59.12	20.00	1.01

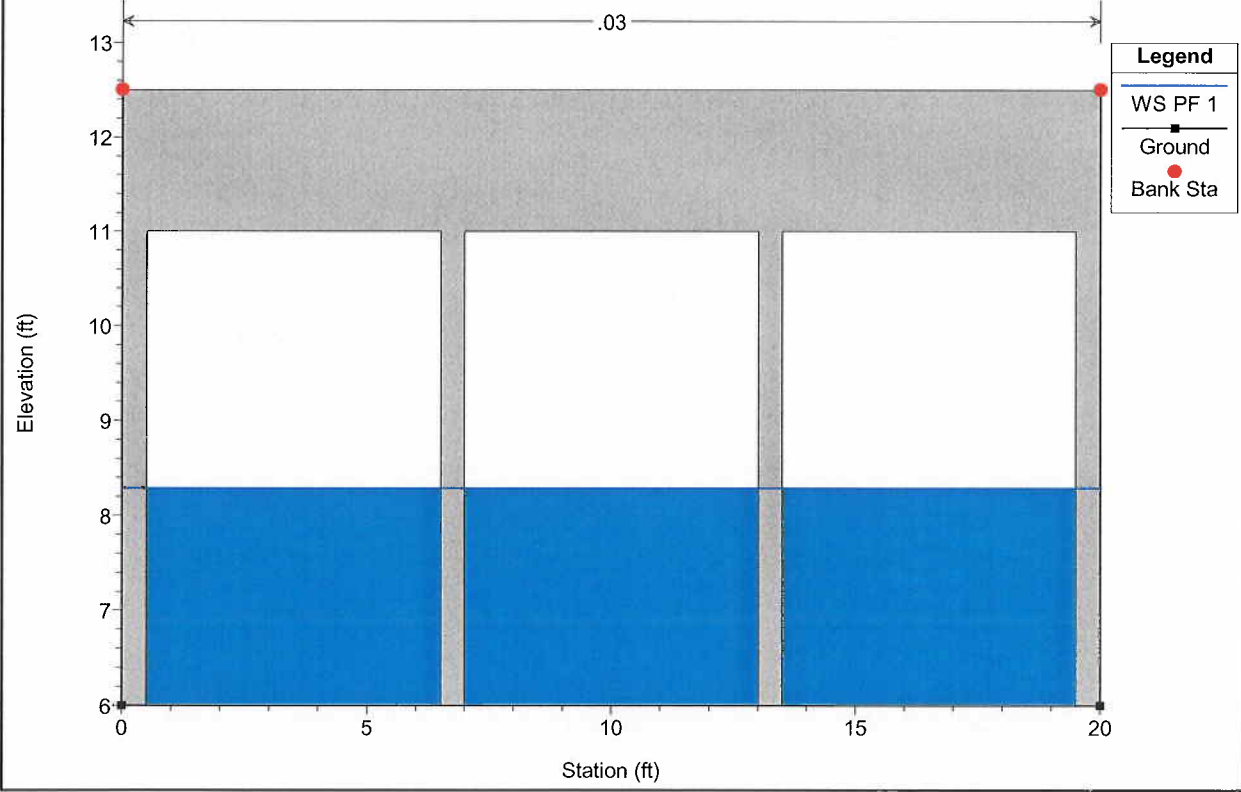
Cottonwood Creek: 48" and 60" RCP Alt.A Plan: 100-Year

RS = 1.5 Culv

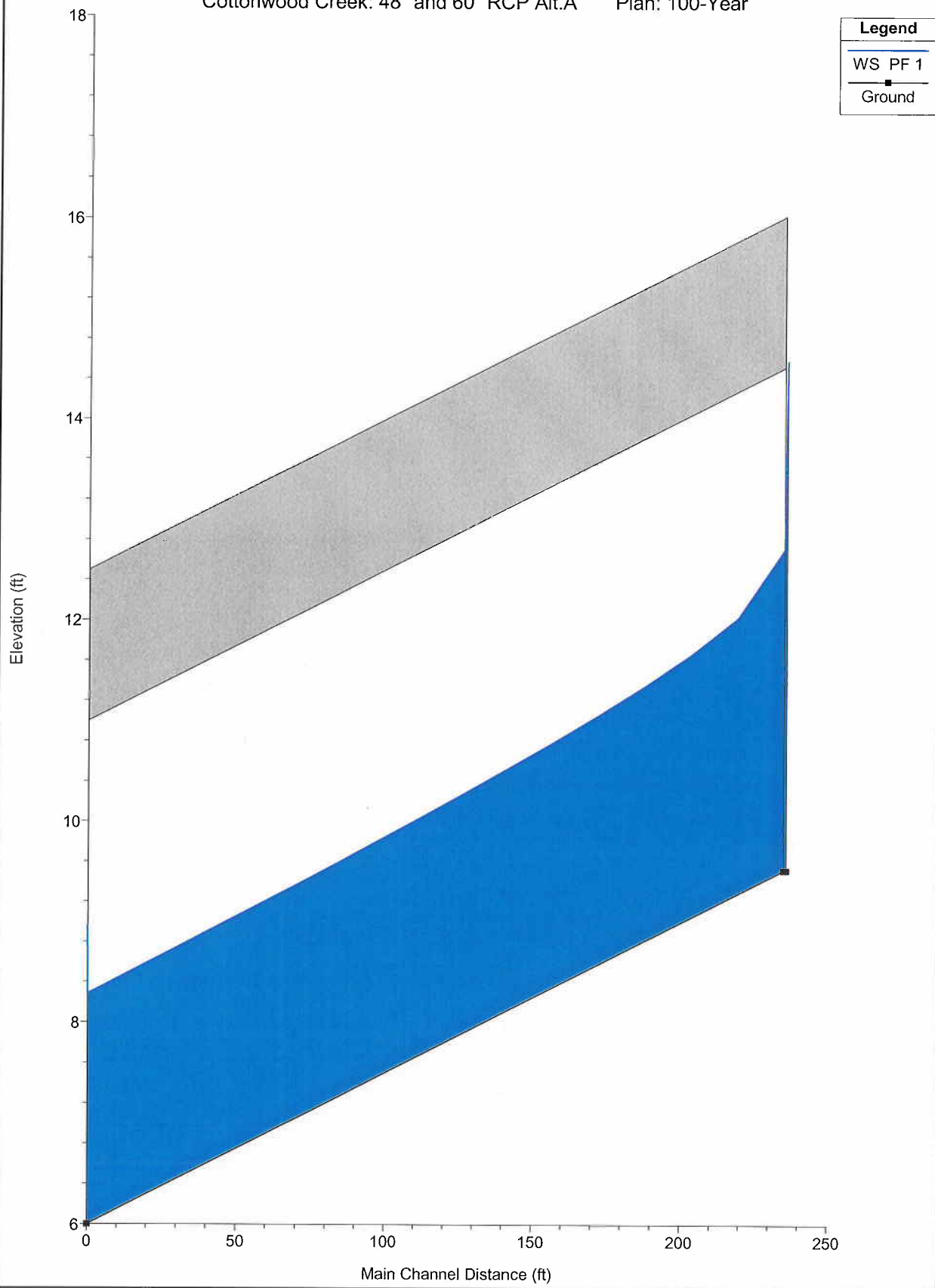


Cottonwood Creek: 48" and 60" RCP Alt.A Plan: 100-Year

RS = 1.5 Culv



Cottonwood Creek: 48" and 60" RCP Alt.A Plan: 100-Year



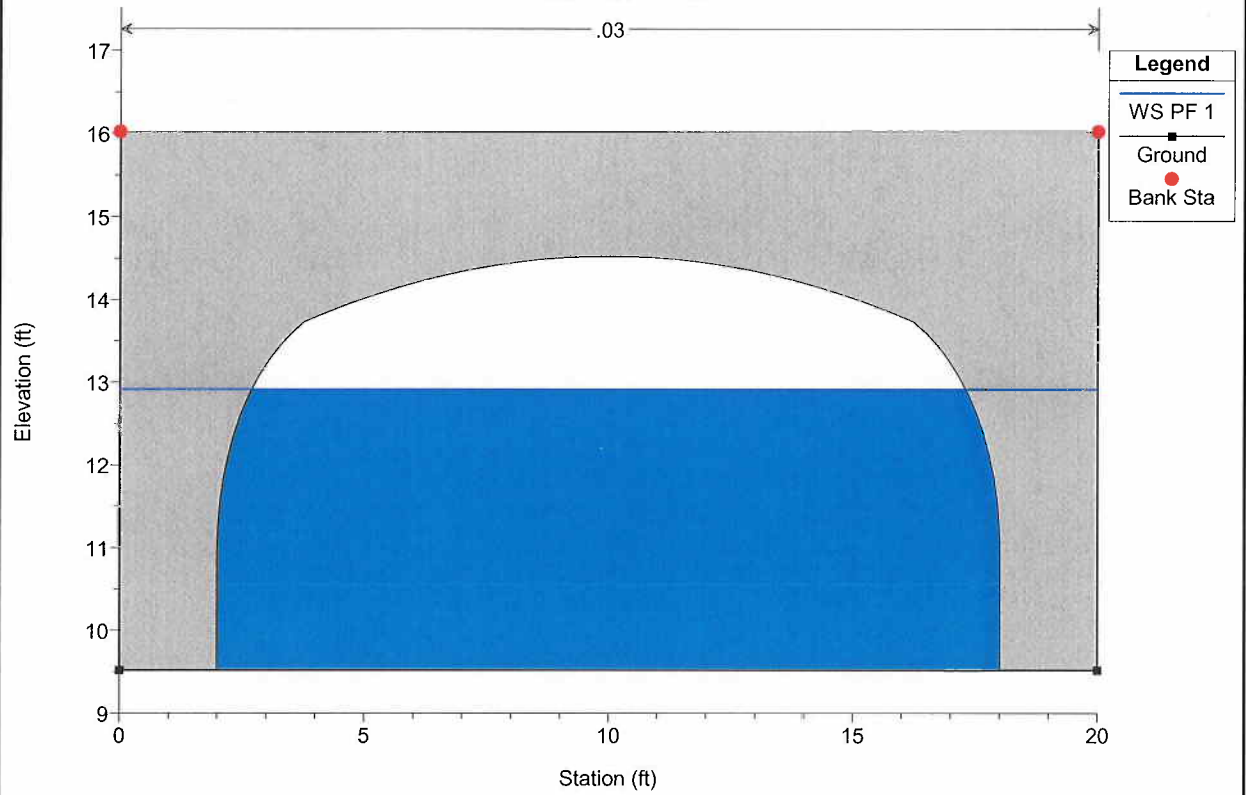
Alternative B: 16' x 5' Conspan Bridge

HEC-RAS Plan: 100-Year River: Cottonwood Creek Reach: Ocean Outfall Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Ocean Outfall	2	PF 1	580.00	9.52	15.26	12.48	15.66	0.001852	5.05	114.84	20.00	0.37
Ocean Outfall	1.5	Culvert										
Ocean Outfall	1	PF 1	580.00	6.00	8.96	8.96	10.45	0.013061	9.81	59.12	20.00	1.01

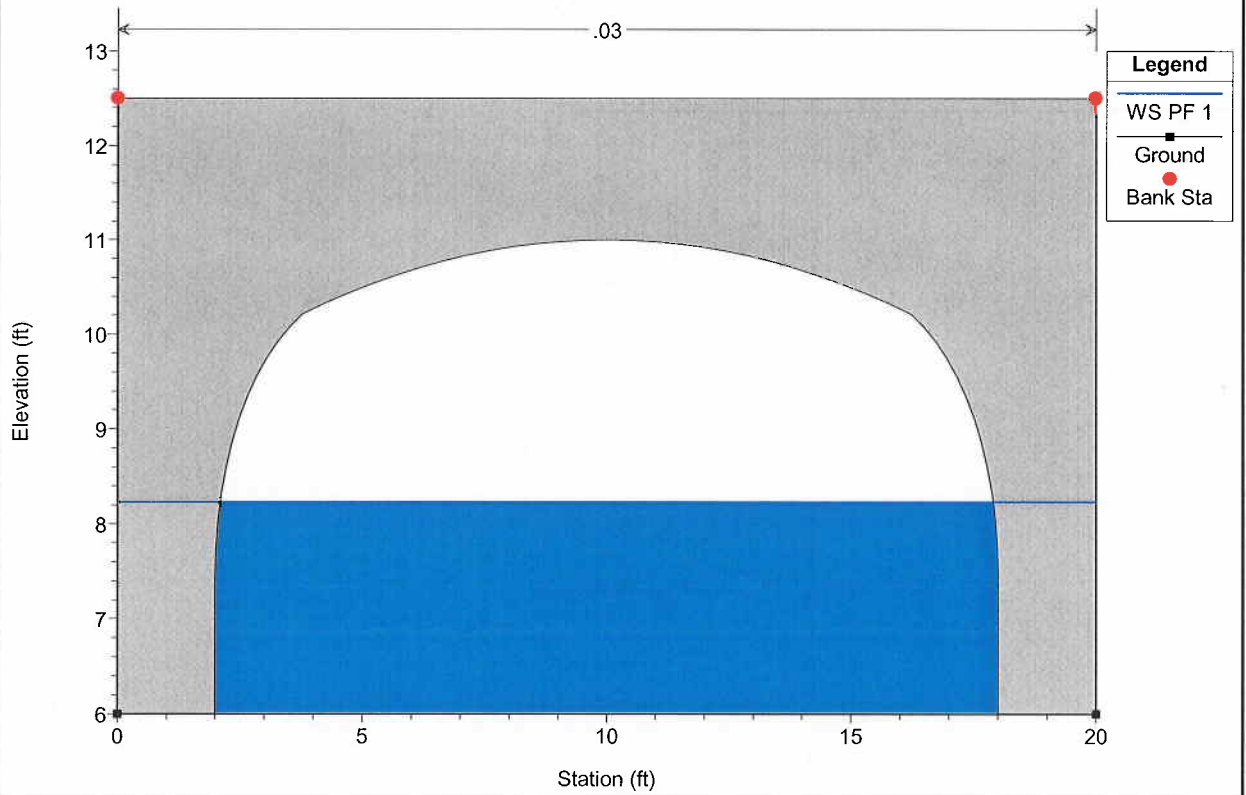
Cottonwood Creek: 48" and 60" RCP Alt.B Plan: 100-Year

RS = 1.5 Culv



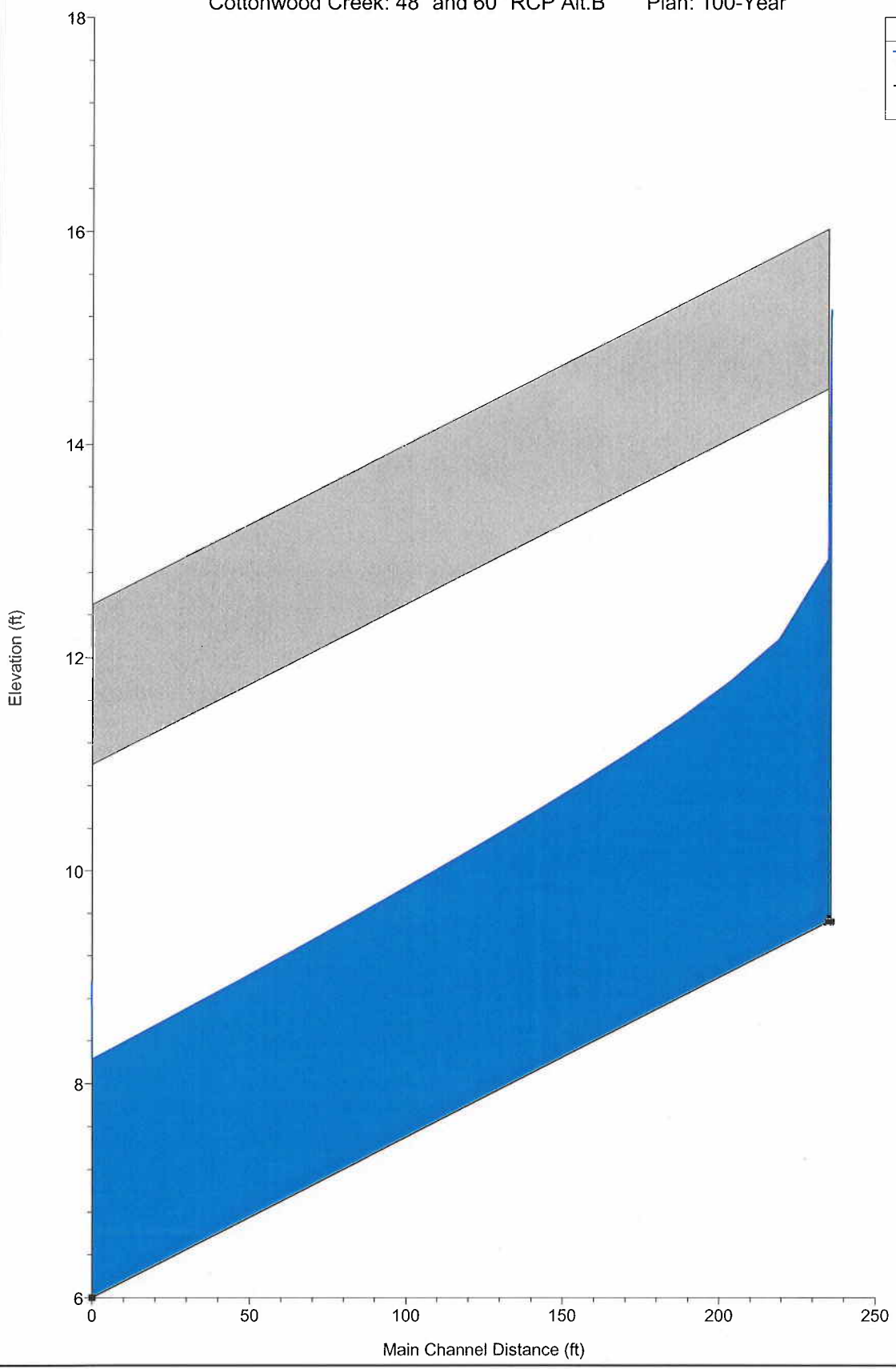
Cottonwood Creek: 48" and 60" RCP Alt.B Plan: 100-Year

RS = 1.5 Culv



Cottonwood Creek: 48" and 60" RCP Alt.B Plan: 100-Year

Legend	
WS PF 1	—
Ground	—■—

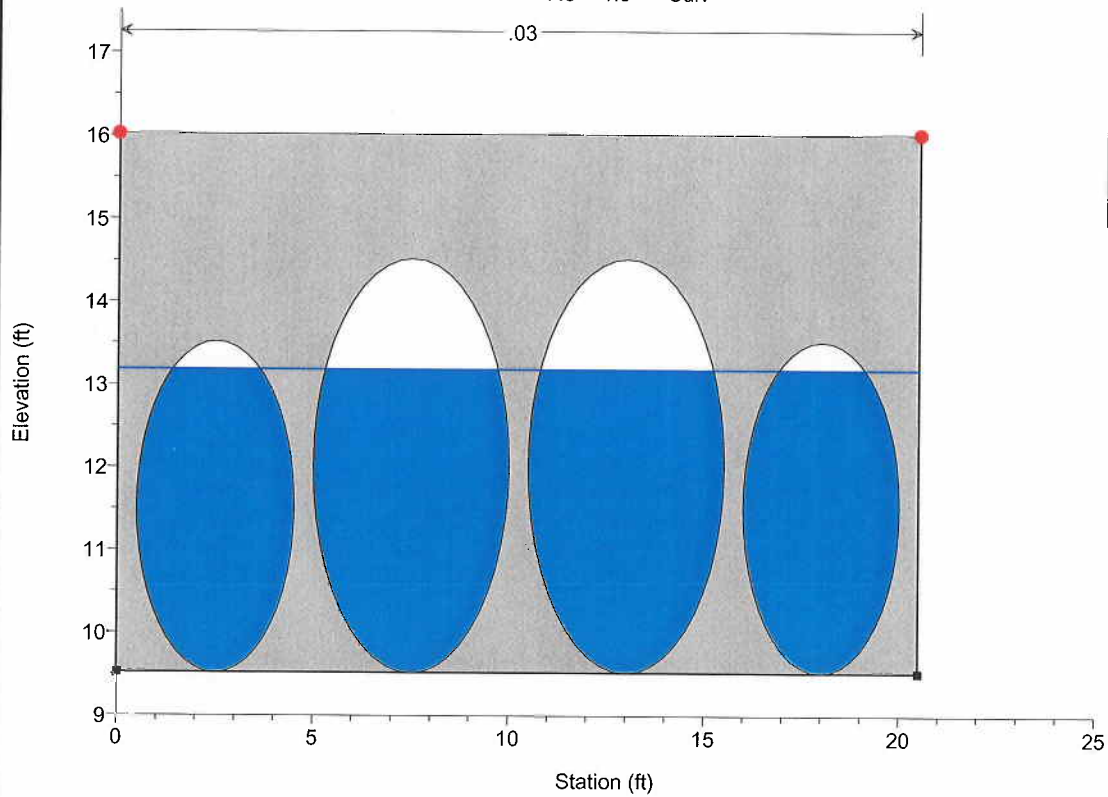


Alternative C: 2- 60" RCP and 48" RCP

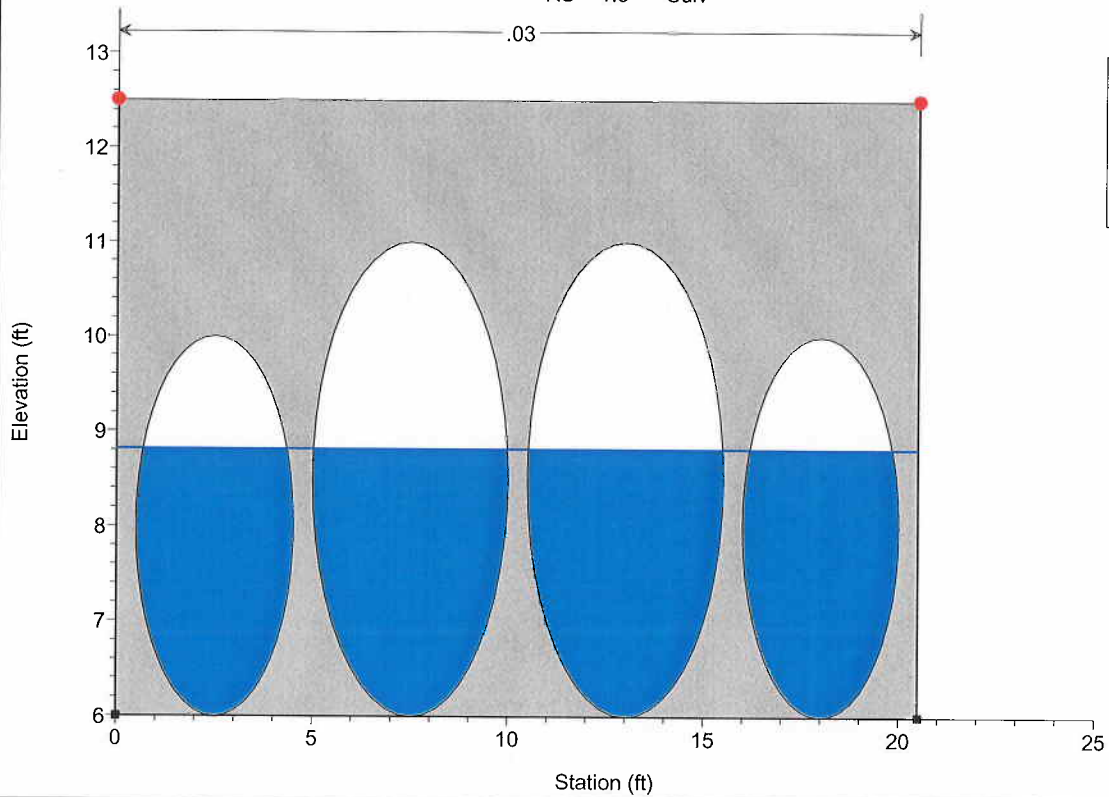
HEC-RAS Plan: 100-Year River: Cottonwood Creek Reach: Ocean Outfall Profile: PF 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chf
Ocean Outfall	2	PF 1	580.00	9.52	15.45	12.43	15.80	0.001588	4.77	121.60	20.50	0.35
Ocean Outfall	1.5	Culvert										
Ocean Outfall	1	PF 1	580.00	6.00	8.91	8.91	10.38	0.012972	9.73	59.61	20.50	1.01

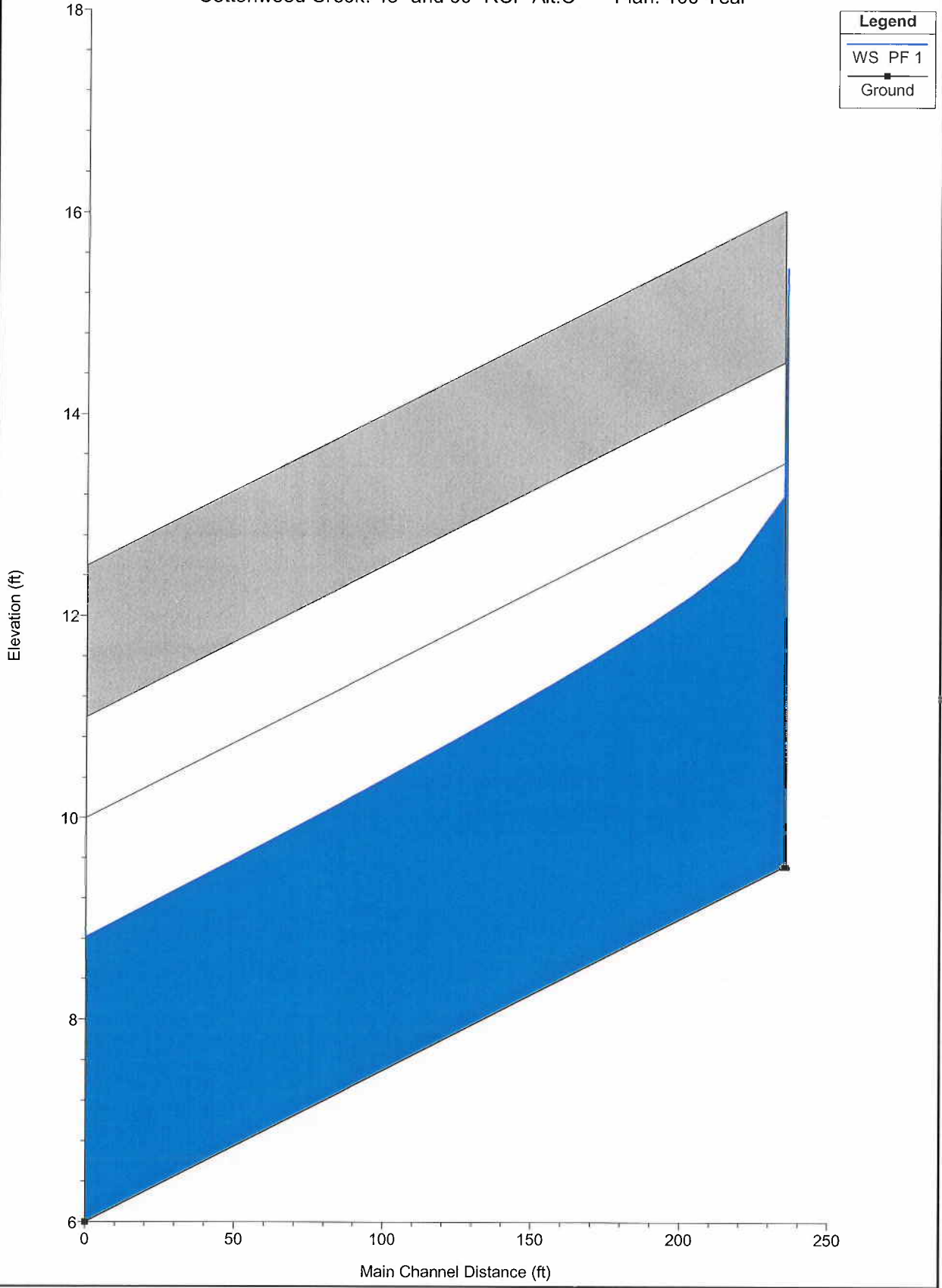
Cottonwood Creek: 48" and 60" RCP Alt.C Plan: 100-Year
RS = 1.5 Culv



Cottonwood Creek: 48" and 60" RCP Alt.C Plan: 100-Year
RS = 1.5 Culv



Cottonwood Creek: 48" and 60" RCP Alt.C Plan: 100-Year



APPENDIX D
PROPOSED FOURTH STREET STORM DRAIN SYSTEM

4th Street Curb Inlets

Worksheet for Curb Inlet On Grade

Project Description	
Worksheet	4th Street Inlets
Type	Curb Inlet On Gr
Solve For	Efficiency

Input Data	
Discharge	50.00 cfs
Slope	007000 ft/ft
Gutter Width	1.33 ft
Gutter Cross Slope	093750 ft/ft
Road Cross Slope	020000 ft/ft
Mannings Coefficient	0.017
Curb Opening Length	65.00 ft
Local Depression	4.0 in
Local Depression \	4.00 ft

Results	
Efficiency	1.00
Intercepted Flow	50.00 cfs
Bypass Flow	0.00 cfs
Spread	34.04 ft
Depth	0.78 ft
Flow Area	11.7 ft ²
Gutter Depression	1.2 in
Total Depression	5.2 in
Velocity	4.29 ft/s
Equivalent Cross Slope	032136 ft/ft
Length Factor	1.02
Total Interception Length	63.50 ft

Stormwater Main Worksheet for Circular Channel

Project Description	
Worksheet	4th Street Mair
Flow Element	Circular Chann
Method	Manning's Forr
Solve For	Channel Depth

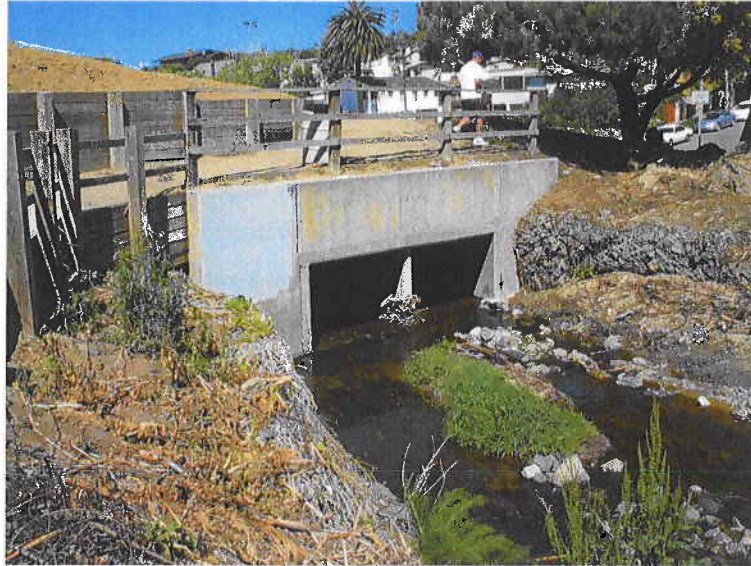
Input Data	
Mannings Coeffic	0.013
Slope	113000 ft/ft
Diameter	36 in
Discharge	100.00 cfs

Results	
Depth	1.40 ft
Flow Area	3.2 ft ²
Wetted Perime	4.52 ft
Top Width	2.99 ft
Critical Depth	2.90 ft
Percent Full	46.8 %
Critical Slope	0.019680 ft/ft
Velocity	30.81 ft/s
Velocity Head	14.75 ft
Specific Energ:	16.16 ft
Froude Numbe	5.22
Maximum Disc	241.17 cfs
Discharge Full	224.20 cfs
Slope Full	0.022481 ft/ft
Flow Type	Supercritical

APPENDIX E
SITE PHOTOGRAPHS

COTTONWOOD CREEK/MOONLIGHT BEACH

Hydrology and Facilities Analysis Summary



Looking downstream at double 6' x 4' RCB that passes under Third Street



Looking downstream at triple 6'-8" x 5' CMPA

COTTONWOOD CREEK/MOONLIGHT BEACH

Hydrology and Facilities Analysis Summary



Looking downstream at 10' x 4' RCB that passes under B Street



Looking downstream at 60" and 48" RCP



Looking upstream at triple 6'-8" x 5' CMPA



Looking upstream at 60" and 48" RCP